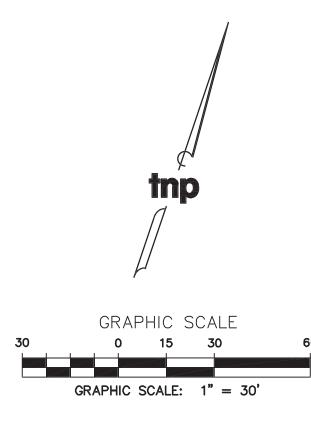
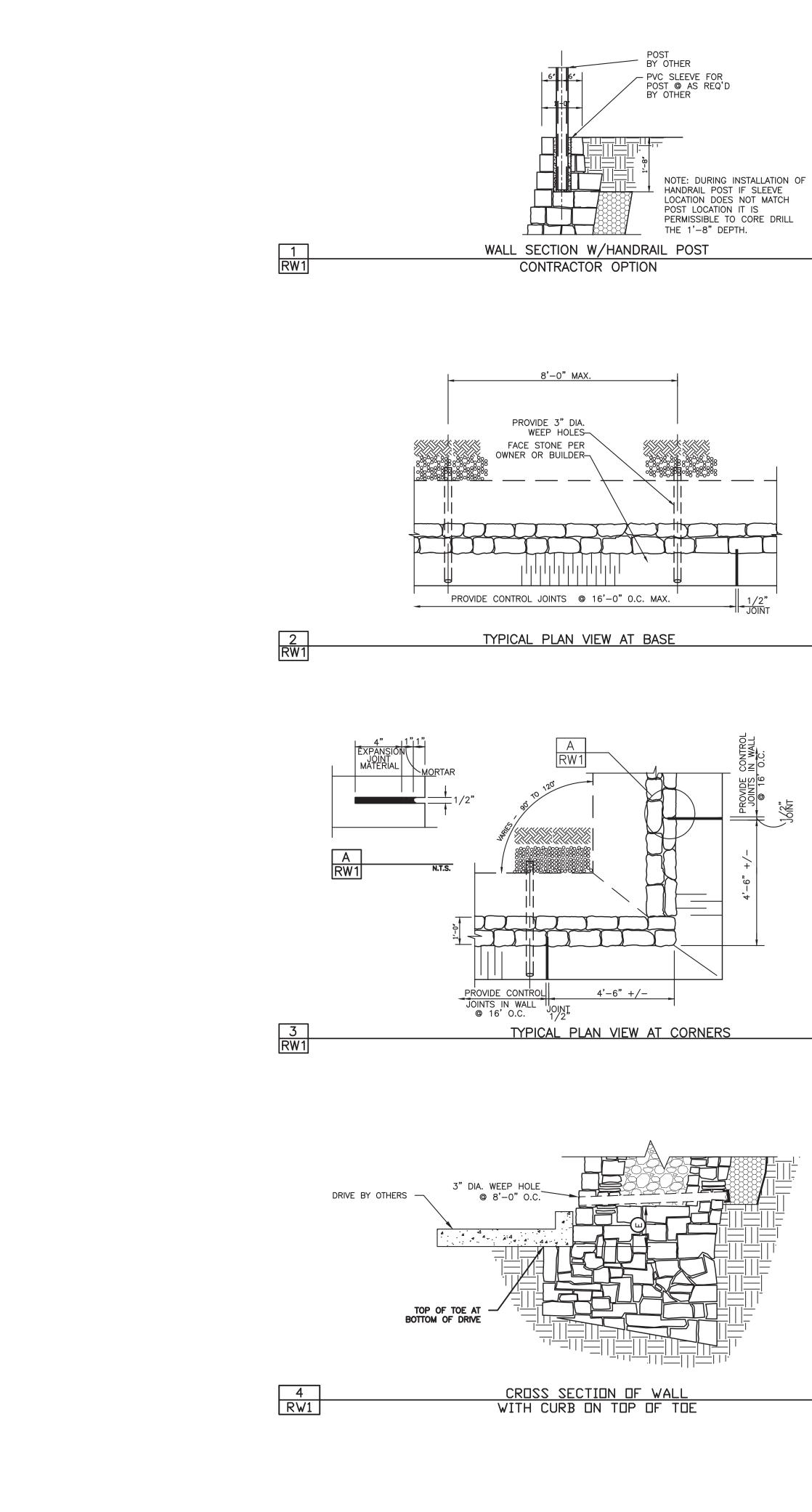


NOTE FROM FALKOFSKE: This plan was developed directly from the Teague Nall and Perkins, Inc. Grading Plan dated February 2020, sheet C1.10. This plan is for the sole purpose of showing what retaining wall sections to use where and to comment on the site as necessary with regards to the retaining walls. Contractor shall review final Civil Plans for other notes with regard to the site prior to constructing Masonry Stone Retaining Walls.

Image: Section of the control of th
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MASONR HARBOR NWC HA NWC HA NWC HA ROCKWA #2 HOF #2 HOF #2 HOF
AARON M. BERKES JOB NO. 748.19
job no. 748.19 SP1
SP1



F



GENERAL NOTES

<u>1. Design</u>

1.1. Design Codes

International Building Code, 2018 Edition

1.2. Geotechnical Report

Firm: ECS Southwest, LLP December 17, 2019 Report No. <u>19:7856</u> Dated: Allowable Bearing Capacity ____

_1500 psf _

1.3. Design Parameters

ngle Cohesion (psf) Unit Weight (pcf)
deg 0 psf	120 pcf
deg 0 psf	120 pcf
	5

Factors of Safety:

External Stability

а.	Minimum Factor of Safety Against Base Sliding (Static Condition)	1.5
b.	Minimum Factor of Safety Against Overturning	2.0

b. Minimum Factor of Safety Against Overturningc. Minimum Factor of Safety Against Global Stability d. Minimum Factor of Safety for Bearing Capacity

Design Loading:

Lateral earth pressures are calculated using Coulombs Lateral Earth Pressure Theory. Designs have been performed to accept loading per the proposed loading conditions based on the Civil Grading Plans. A live loading of 250 psf has been used for all walls supporting areas subject to firelane loading.

1.5

3.0

Retaining walls should not have solid fence (such as wood fence) placed on top of wall other than that shown on these plans. Retaining walls shall not have additional surcharge placed above wall other than that shown on these plans. Retaining walls shall not have slope at base or top of wall that exceed that which is shown on these plans. The retaining walls noted above require special design.

2. Materials

2.1. Soil Types

a. Retained Backfill

a.a. On site clayey soils a.b. Properly compacted on-site fill soils, verification by others.

- b. Foundation Soils (Allowable Bearing = 1500 psf min)
- b.a. Bearing on Stiff Natural Undisturbed Clayey or Sandy Soils or Compacted and Tested Fill Soils
- b.b. Friction Angle between Base of Wall and Soil 17 deg b.c. Bearing in fill soils. Fill soils supporting the retaining walls shall be placed in accordance with the recommendations for the fill placement per the geotechincal report.
- c. Drainage Material

c.a. Free draining granular backfill, clean, non-plastic, relatively well-graded.

2.2. Dimension Stone

- a. Average Density of masonry wall varies from 135pcf to 145pcf.
- b. Stone size varies from 4" to 18". c. Face stone shall be coordinated between contractor and owner/developer.
- d. Recycled concrete 4" to 18" may be used in place of dimension stone, contractors option.

2.3. Rebar/Welded Wire Fabric (If Required)

- a. All steel reinforcement shall be new billet steel conforming to ASTM A-615, Grade 60 with fy=60ksi.
- b. All reinforcement shall not have deleterious material on it.
- c. All welded wire fabric shall have minimum fy=65ksi and be hot dip galvanized.

2.4. Drainage Materials

- a. Weep pipes shall be PVC or corrugated HDPE pipe.
- b. Drainage zone shall be separated from retained backfill by mirafi 140N filter fabric or approved equal.

2.5 Portland Cement Mortar for Retaining Wall Construction.

The portland cement mortar used for construction of the masonry stone retaining walls shall be provided with the following proportions per cubic yard of concrete. The portland cement mortar supplier shall provide "batch tickets" clearly indicating that the appropriate amount of materials are provided in each truck load. The batch tickets shall clearly indicate the amount batched, the date, the project name and shall be provided to Falkofske Engineering, Inc. for review, documentation, and file.

Contents	Amount per cubic yard	Specific Gravity	Volume ft^3
Type 1 Portland cement:	451 lbs	3.15	2.29
Type F Fly Ash	113 lbs	2.93	0.62
Fine Aggregate (sand):	2746 lbs	2.59	16.99
Potable Water	367 lbs	44 Gallons	5.88
Sika Air (or equivalent)	(AS REQ'D) oz	4.5%	1.22
			27.0 Total

Note: the portland cement mortar supplier material weights may vary slightly based on the specific gravity of the materials used.

Concrete retarders may be used at the discretion of the masonry wall contractor. A greater amount of retarder is typically used during hot periods and a less amount of retarder is typically used during cool weather.

Please note that the above proportions will provide a portland cement mortar with a compressive strength of about fc = 2500 psi. Falkofske Engineering, Inc. does not require any concrete testing provided the above proportions are verified by way of the "batch

3. Construction

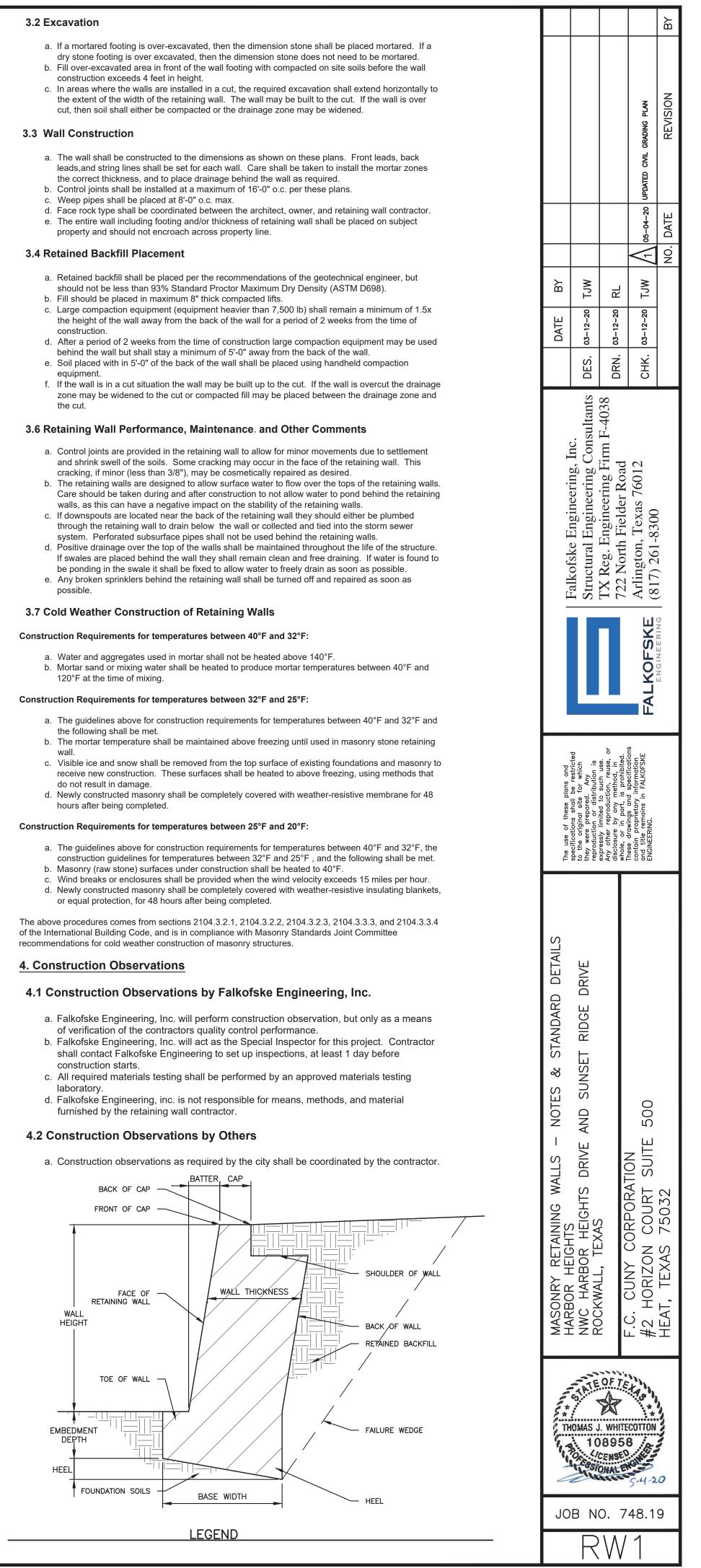
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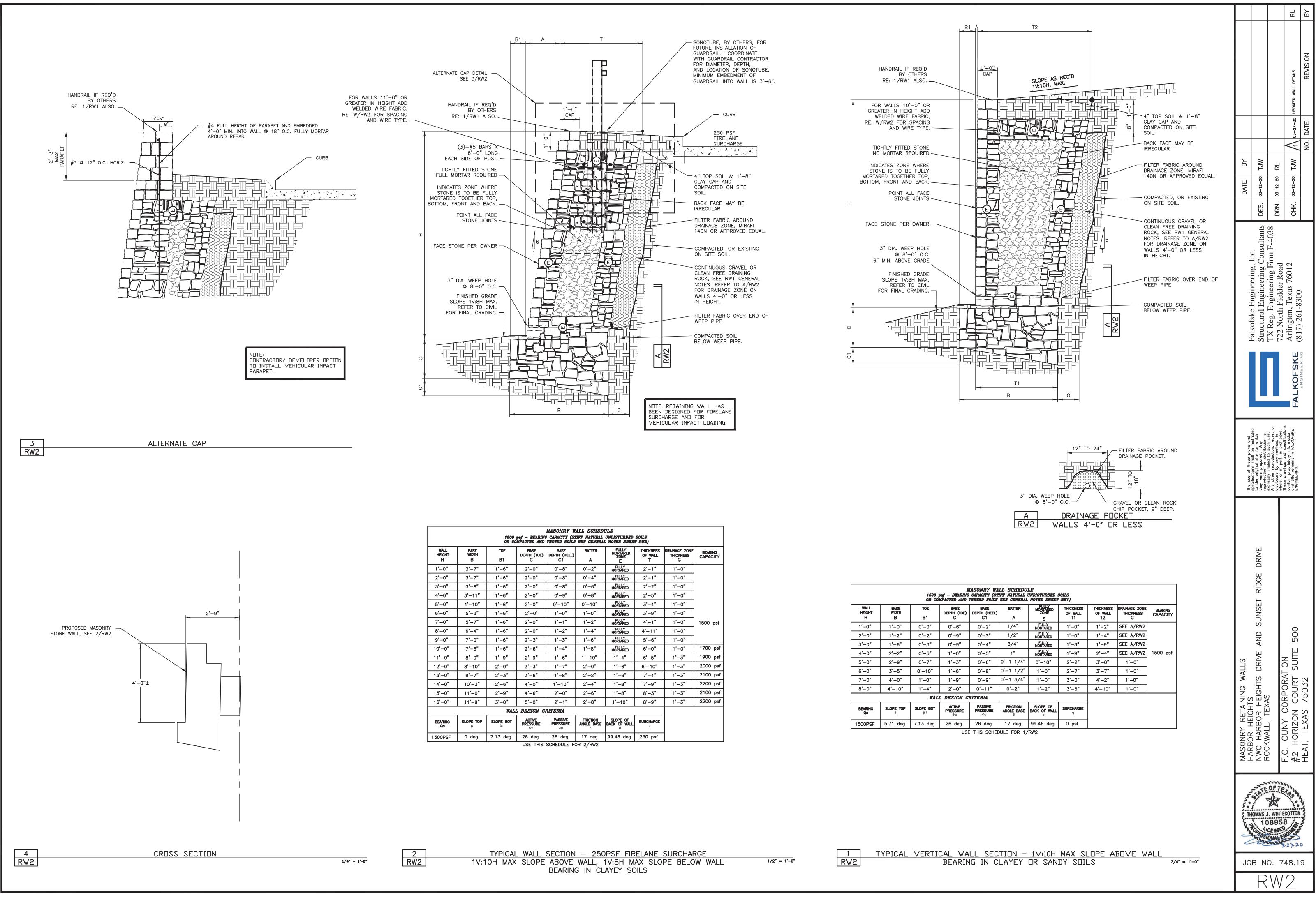
3.1 Preparation Work

- a. Prior to grading or excavation of the site, confirm the location of the retaining walls and all underground features, including utility location within the area of construction. Ensure
- surrounding structures are protected from effects of wall excavation, and construction.
- b. Coordinate installation of underground utilities and other improvements with wall installation.

N.T.S.

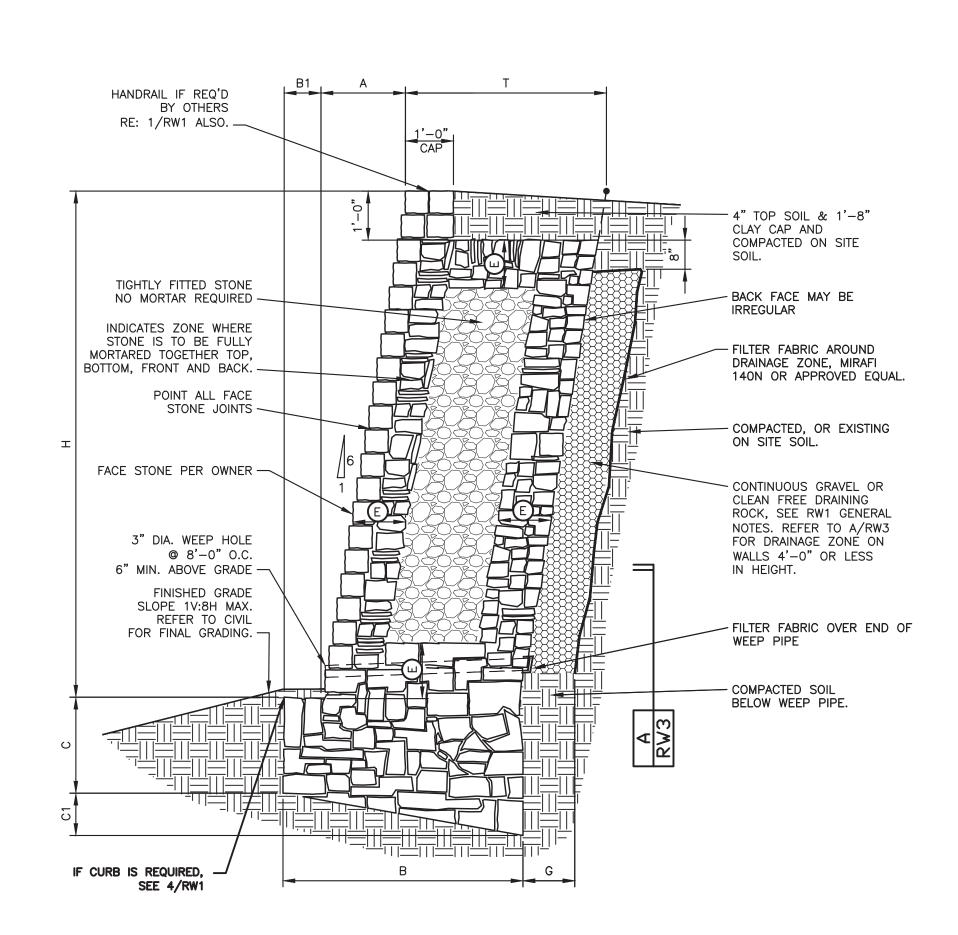
N.T.S.





MASONRY WALL SCHEDULE 1500 pag – Bearing Capacity (Stiff Natural Undisturbed Soils OR COMPACTED AND TESTED SOILS SEE GENERAL NOTES SHEET RW2)													
WALL HEIGHT H	BASE WIDTH B	toe B1	BASE DEPTH (TOE) C	BASE DEPTH (HEEL) C1	batter A	FULLY MORTARED ZONE E	THICKNESS OF WALL T	DRAINAGE ZONE THICKNESS G	BEARING CAPACITY				
1'-0"	3'-7"	1'-6"	2'-0"	0'-8"	0'-2"	FULLY MORTARED	2'-1"	1'-0"					
2'-0"	3'-7"	1'-6"	2'-0"	0'-8"	0'-4"	FULLY MORTARED	2'-1"	1'-0"					
3'-0"	3'-8"	1'-6"	2'-0"	0'-8"	0'-6"	FULLY MORTARED	2'-2"	1'-0"					
4'—0"	3'-11"	1'-6"	2'-0"	0'-9"	0'-8"	FULLY MORTARED	2'-5"	1'-0"					
5'-0"	4'-10"	1'-6"	2'-0"	0'-10"	0'-10"	FULLY MORTARED	3'-4"	1'-0"					
6 ' —0"	5'–3"	1'-6"	2'-0'	1'-0"	1'-0"	FULLY MORTARED	3'-9"	1'-0"					
7'—0"	5 ' -7"	1'-6"	2'-0"	1'-1"	1'-2"	FULLY MORTARED	4'-1"	1'-0"	1500 psf				
B'-0 "	6'-4"	1'-6"	2'-0"	1'-2"	1'-4"	FULLY MORTARED	4'-11"	1'-0"					
9'—0"	7'-0"	1'-6"	2'-3"	1'—3"	1'-6"	FULLY MORTARED	5'-6"	1'-0"					
0'-0"	7'-6"	1'-6"	2'-6"	1'-4"	1'-8"	FULLY MORTARED	6 ' -0"	1'-0"	1700 psf				
1'-0"	8'-0"	1'—9"	2'-9"	1'-6"	1'-10"	1'-4"	6'-5"	1'-3"	1900 psf				
2'-0"	8'-10"	2'-0"	3'–3"	1'-7"	2'-0"	1'-6"	6'-10"	1'-3"	2000 psf				
3'-0"	9'-7"	2'-3"	3'-6"	1'-8"	2'-2"	1'-6"	7'-4"	1'-3"	2100 psf				
4'-0"	10'-3"	2'-6"	4'-0"	1'-10"	2'-4"	1'-8"	7'–9"	1'-3"	2200 psf				
5'-0"	11'-0"	2'-9"	4'-6"	2'-0"	2'-6"	1'-8"	8 ' -3"	1'-3"	2100 psf				
6'-0"	11'-9"	3'-0"	5'-0"	2'-1"	2'-8"	1'-10"	8'-9"	1'-3"	2200 psf				
		WALI	L DESIGN C	RITERIA									
BEARING Qa	SLOPE TOP β	SLOPE BOT β1	ACTIVE PRESSURE ©a	PASSIVE PRESSURE Φp	FRICTION ANGLE BASE o	SLOPE OF BACK OF WALL a	SURCHARGE q						
00PSF	0 deg	7.13 deg	26 deg	26 deg	17 deg	99.46 deg	250 psf						

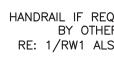
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1'-0" 1'-0" 0'-0" 2'-0" 1'-2" 0'-2" 3'-0" 1'-6" 0'-3" 4'-0" 2'-2" 0'-5" 5'-0" 2'-9" 0'-7" 6'-0" 3'-5" 0'-10" 7'-0" 4'-0" 1'-0" 8'-0" 4'-10" 1'-4" BEARING QG QG β SLOPE TOP β			TOE
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Н	В	B1
3'-0" $1'-6"$ $0'-3"$ $4'-0"$ $2'-2"$ $0'-5"$ $5'-0"$ $2'-9"$ $0'-7"$ $6'-0"$ $3'-5"$ $0'-10"$ $7'-0"$ $4'-0"$ $1'-0"$ $8'-0"$ $4'-10"$ $1'-4"$ BEARING Qg SLOPE TOP BEARING BE	1'-0"	1'-0"	0'-0"
4'-0" 2'-2" 0'-5" 5'-0" 2'-9" 0'-7" 6'-0" 3'-5" 0'-10" 7'-0" 4'-0" 1'-0" 8'-0" 4'-10" 1'-4" BEARING Qa SLOPE TOP β 9	2'-0"	1'-2"	0'-2"
5'-0" 2'-9" 0'-7" 6'-0" 3'-5" 0'-10' 7'-0" 4'-0" 1'-0" 8'-0" 4'-10" 1'-4" BEARING Qa SLOPE TOP β SLOPE BO β 1 β 1	3'-0"	1'-6"	0'-3"
6'-0" 3'-5" 0'-10' 7'-0" 4'-0" 1'-0" 8'-0" 4'-10" 1'-4" BEARING Qa SLOPE TOP β SLOPE BC β 1	4'-0"	2'-2"	0'-5"
7'-0" 4'-0" 1'-0" 8'-0" 4'-10" 1'-4" BEARING Qa SLOPE TOP β SLOPE BG $\beta1$	5'-0"	2'-9"	0'-7"
8'-0" 4'-10" 1'-4" ΒΕΑRING Qa SLOPE TOP β SLOPE BC β SLOPE TOP	6'-0"	3'-5"	0'-10"
BEARING Qα SLOPE TOP β β β	7'-0"	4'-0"	1'-0"
BEARING SLOPE TOP SLOPE BC Qα β β1	8'-0"	4'-10"	1'-4"
Qa β β1			WA
1500PSF 5.71 deg 7.13 de			SLOPE BOT β1
•	1500PSF	5.71 deg	7.13 deg

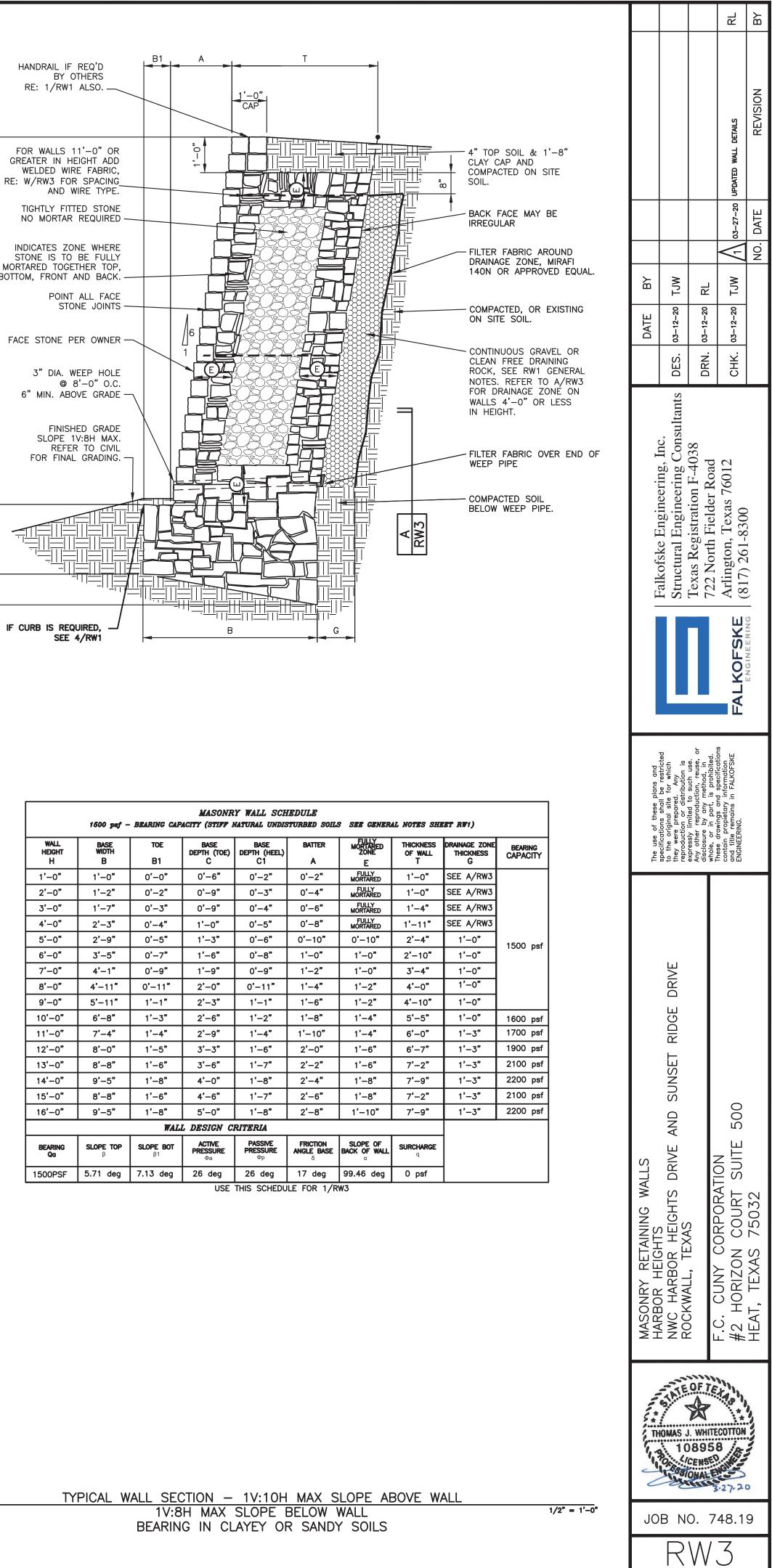


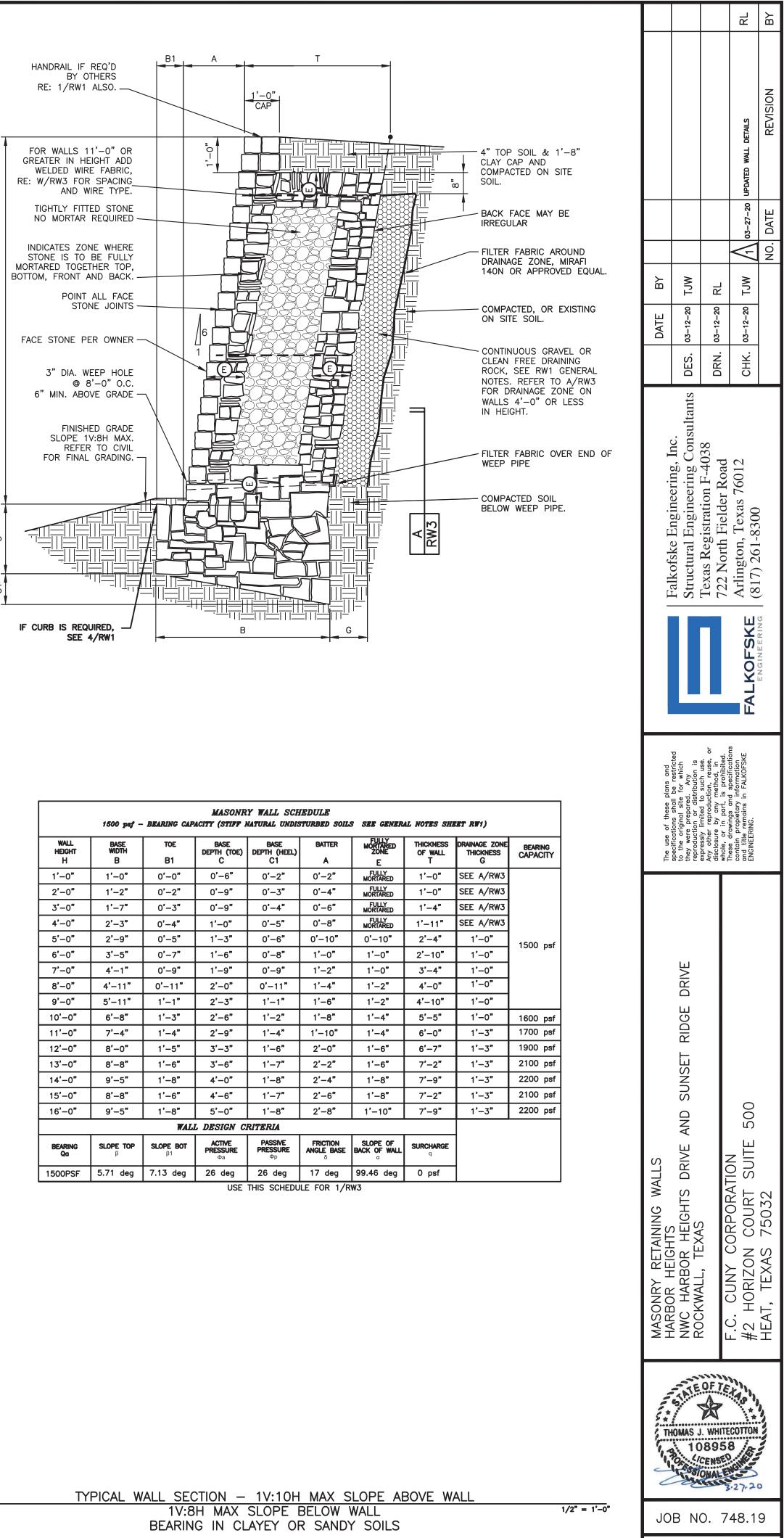
WALL HEIGHT H	BASE WIDTH B	TOE B1	BASE DEPTH (TOE) C	BASE DEPTH (HEEL) C1	BATTER	FULLY MORTARED ZONE E	THICKNESS OF WALL T	DRAINAGE ZONE THICKNESS G	BEARING CAPACIT
1'-0"	1'-0"	0'-0"	0'-6"	0'-2"	0'-2"	FULLY MORTARED	1'-0"	1'-0"	
2'-0"	1'-4"	0'-2"	0'-9"	0'-3"	0'-4"	FULLY MORTARED	1'-2"	1'-0"	
3'-0"	1'-9"	0'-3"	1'-0"	0'-4"	0'-6"	FULLY MORTARED	1'-6"	1'-0"	
4'-0"	2'-7"	0'-4"	1'-3"	0'-6"	0'-8"	FULLY MORTARED	2'-3"	1'-0"	1500 p:
5 ' -0"	3'-3"	0'-5"	1'-6"	0'-7"	0'-10"	0'-10"	2'-10"	1'-0"	
6'-0"	4'-0"	0'-7"	2'-0"	0'-9"	1'-0"	1'-0"	3'-5"	1'-0"	
7'-0"	4'-10"	0'-9"	2'-3"	0'-10"	1'-2"	1'-0"	4'-1"	1'-0"	
8'-0"	5'-8"	0'-10"	2'-9"	1'-0"	1'-4"	1'-2"	4' -10"	1'-0"	
9'-0"	6'-10"	0'-11"	3'-3"	1'–3"	1'-6"	1'-2"	5'–11"	1'-0"	
10'-0"	7'-7"	1'-0"	3'-9"	1'-5"	1'-8"	1'-4"	6'-7"	1'-0"	1700 p:
		WAL	L DESIGN C.	RITERIA					
BEARING Qa	SLOPE TOP β	SLOPE BOT β1	ACTIVE PRESSURE ©a	PASSIVE PRESSURE ^{Φp}	FRICTION ANGLE BASE o	SLOPE OF BACK OF WALL	SURCHARGE q		
1500PSF	14 deg	7.13 deg	26 deg	26 deg	17 deg	99.46 deg	0 psf	1	

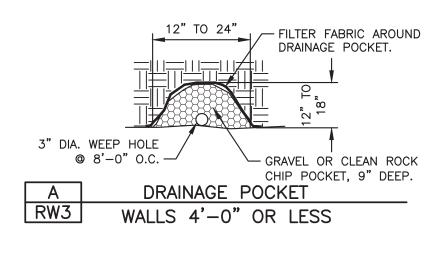
TYPICAL WALL SECTION
BEARING IN CLAYS
MAX. SLOPE ABOVE WALL 1V:4H
MAX. SLOPE BELOW WALL 1V:8H

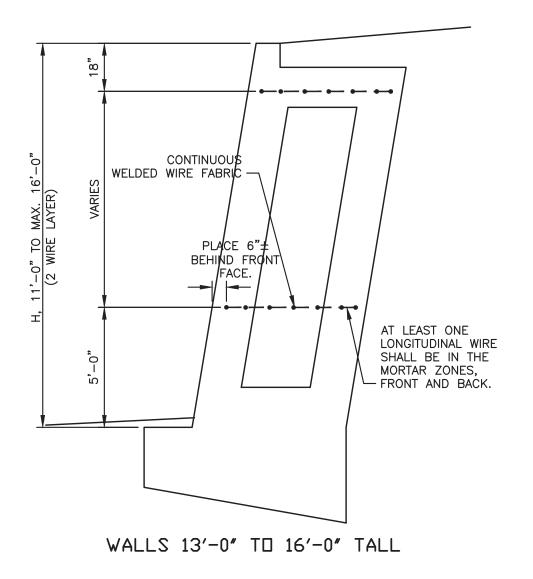
2 RW3

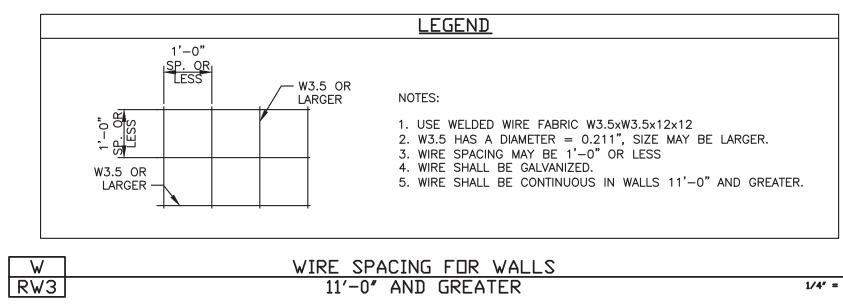






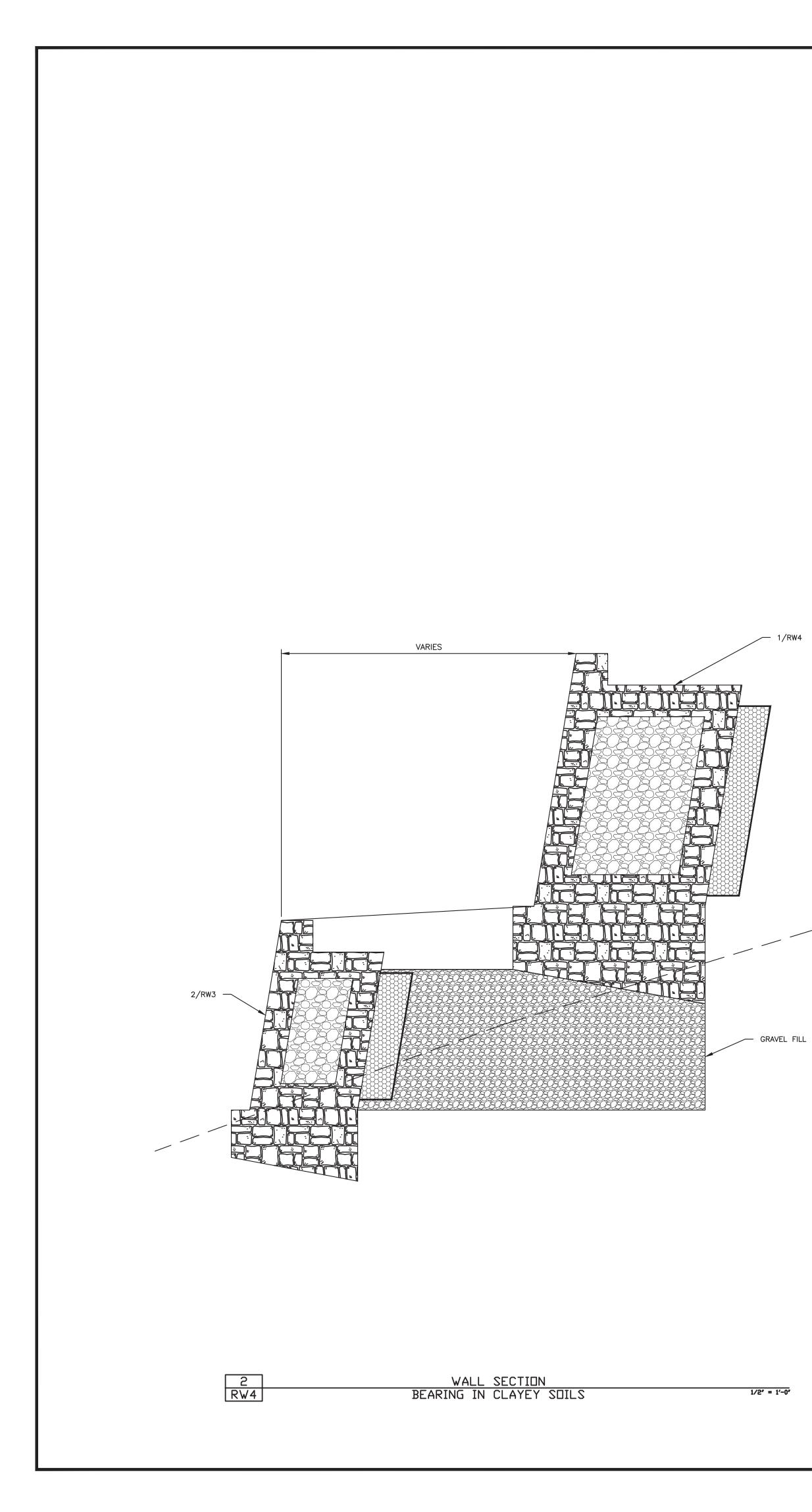






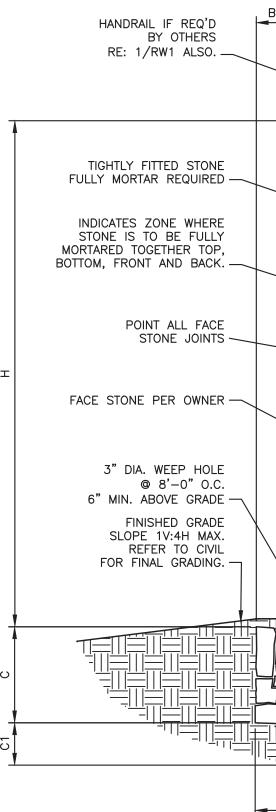
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1 RW3

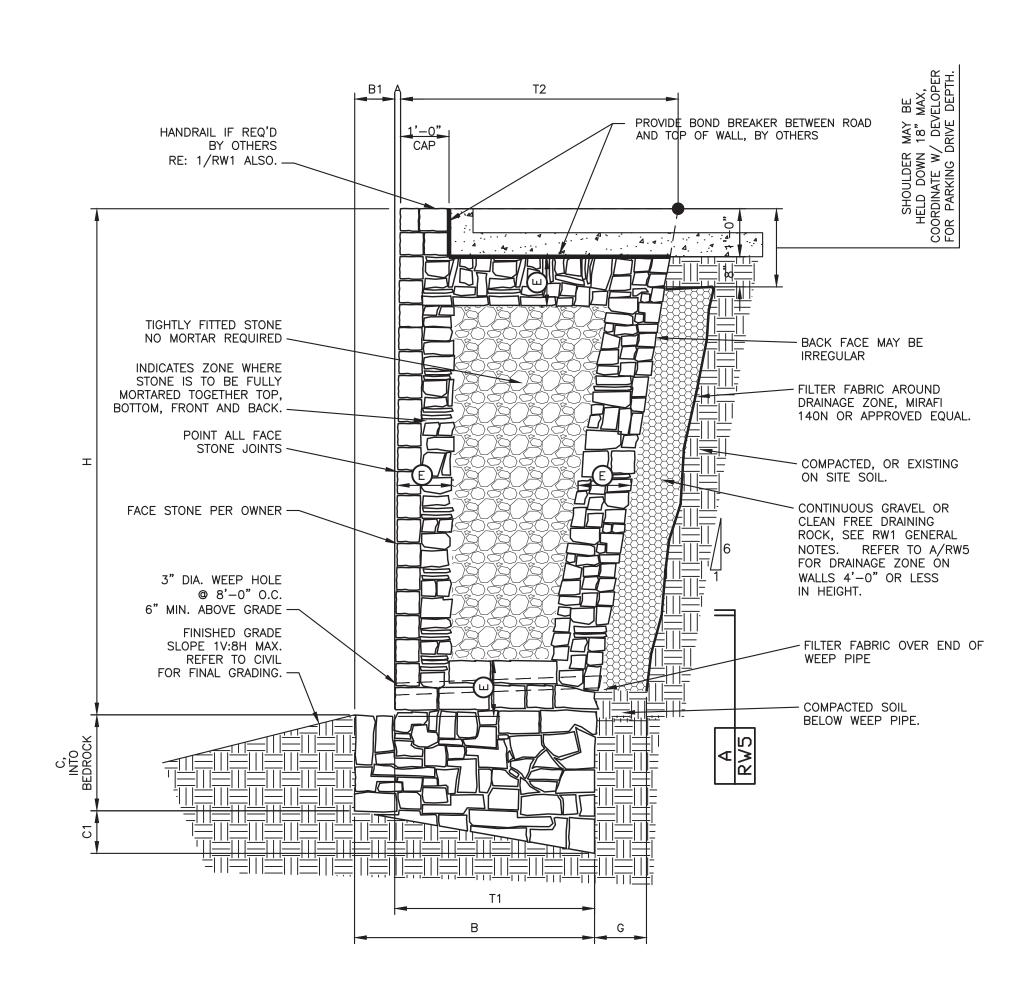


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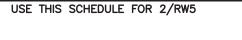
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4'-0" 2'-9"	0'-4"	1'-6" 1'-9"	0'-6"	0'-8"	FULLY MORTARED	2'-5"	SEE A/RW4 1'-0"	1500 psf			AND		500	
5'-0" 3'-6" 6'-0" 4'-3"	0'-5" 0'-6"	1 -9 2'-3"	0'-8" 0'-9"	0'-10" 1'-0"	0'-10" 1'-0"	3'-1" 3'-9"	1'-0"	1000 par		S	DRIVE	Z	SUITE	
7'-0" 5'-2" 8'-0" 6'-1"	0'-7" 0'-8"	2'-6" 3'-0"	0'-11" 1'-1"	1'-2" 1'-4"	1'-0" 1'-2"	4'-7" 5'-5"	1'-0" 1'-0"			WALLS	DR		S IS	
9'-0" 7'-3"	0'-9"	3'-3"	1'-3"	1'-6"	1'-2"	6'-6"	1'-0"			≥ ()	HTS	A A A)32
		DESIGN C	RITERIA PASSIVE	FRICTION	SLOPE OF		-			NIN N	RBOR HEIGHTS LL, TEXAS	dad		750
Qα β	SLOPE BOT β1	ACTIVE PRESSURE ©a	PRESSURE ^{Φp}	δ	SLOPE OF BACK OF WALL a	g g				ETAI	TEX F	C		St
1500psf 14 deg	14 deg	26 deg USE	26 deg THIS SCHEDU	17 deg JLE FOR 1/F	99.46 deg RW4	0 psf					HARBOR WALL, TE	×NI C	RIZON	EX
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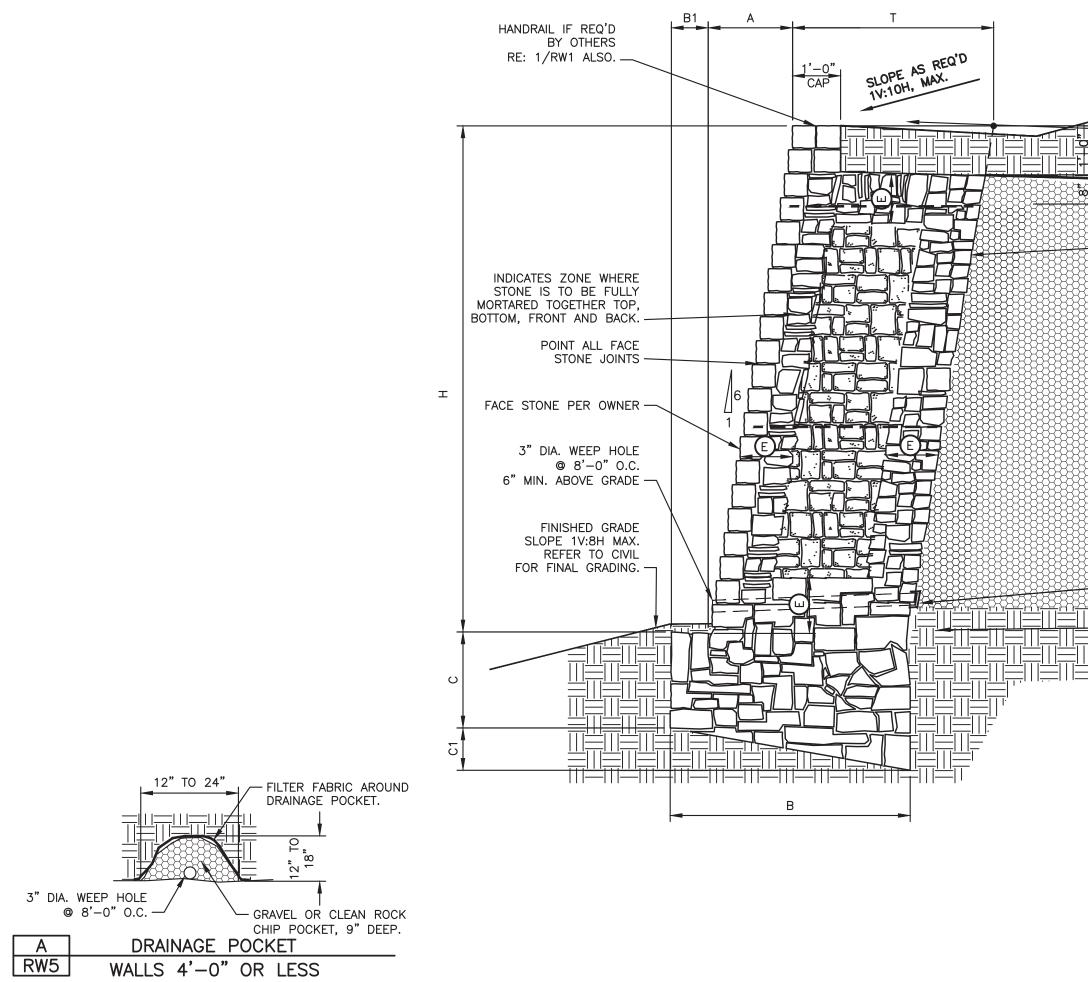


	MASONRY WALL SCHEDULE 1500 psf – BEARING CAPACITY (STIFF NATURAL UNDISTURBED SOILS OR COMPACTED AND TESTED SOILS SEE GENERAL NOTES SHEET RW1)											
WALL HEIGHT H	BASE WIDTH B	toe B1	BASE DEPTH (TOE) C	BASE DEPTH (HEEL) C1	batter A	FULLY MORTARED ZONE E	THICKNESS OF WALL T1	THICKNESS OF WALL T2	DRAINAGE ZONE THICKNESS G	BEARING CAPACITY		
1'-0"	1'-9"	0'-2"	1'-0"	0'-4"	1/4"	FULLY MORTARED	1'-7"	1'-9"	SEE A/RW5			
2'-0"	2'-3"	0'-3"	1'-0"	0'-5"	1/2"	FULLY MORTARED	2'-0"	2'-4"	SEE A/RW5			
3'-0"	2'-9"	0'-4"	1'-0"	0'-6"	3/4"	FULLY MORTARED	2'-5"	2'-11"	SEE A/RW5	1500 psf		
4'-0"	3'-4"	0'-7"	1'-0"	0'-8"	0'-1"	FULLY MORTARED	2'-9"	3'-5"	SEE A/RW5	•		
5'-0"	4'-0"	0'-8"	1'-3"	0'-9"	0'-1 1/4"	0'-8"	3'-4"	4'-2"	1'-0"			
6'-0"	4'-7"	0'-10"	1'-6"	0'-10"	0'-1 1/2"	0'-10"	3'-9"	4'-9"	1'-0"			
		WAL	L DESIGN C	RITERIA	<u>.</u>	•						
BEARING Qa	SLOPE TOP β	SLOPE BOT β1	ACTIVE PRESSURE Φ_a	PASSIVE PRESSURE Φp	FRICTION ANGLE BASE ō	SLOPE OF BACK OF WALL	SURCHARGE q					
1500PSF	0 deg	7.13 deg	26 deg	26 deg	17 deg	99.46 deg	250 psf					





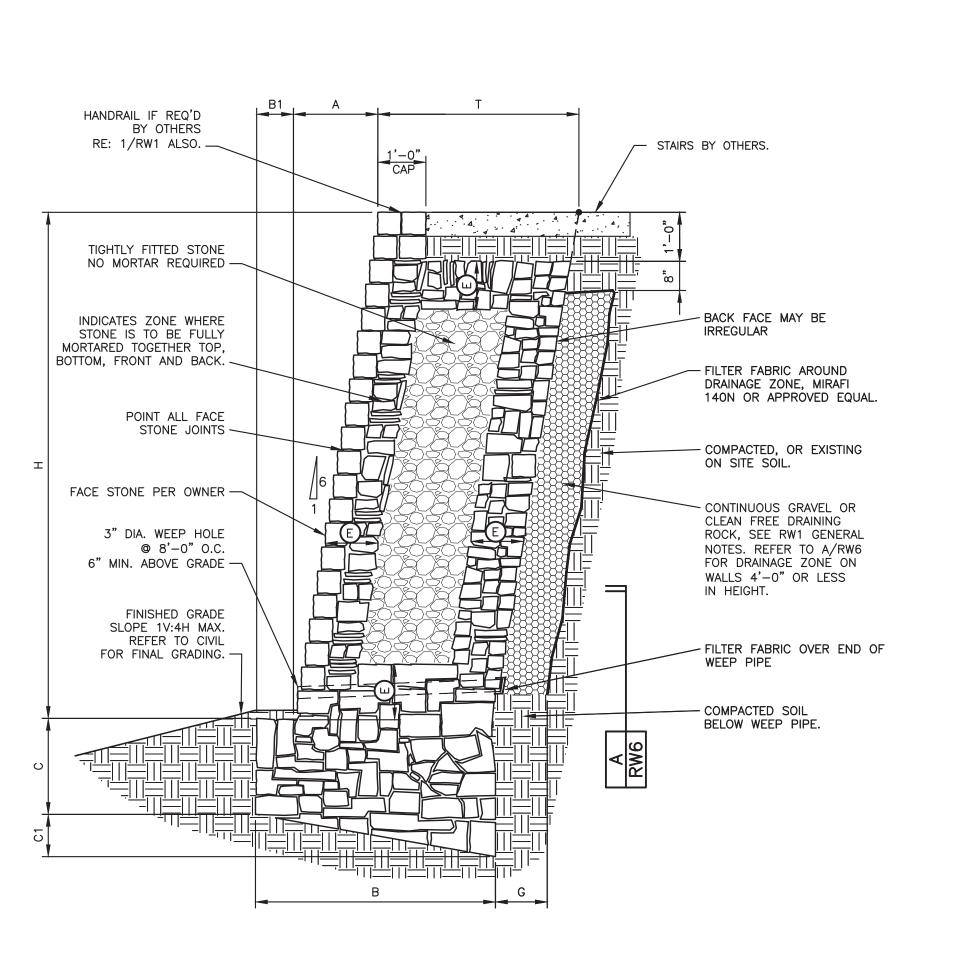
 $3/4^{*} = 1'-0^{*}$

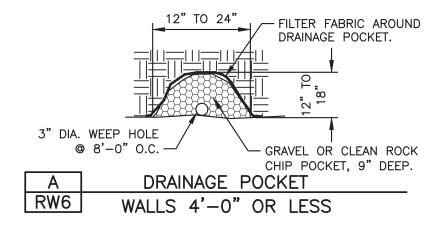


			RL	RL	ΒΥ
T UPPER AS REQ'D IV: OH, MAX.			-08-20 UPDATED WALL DETAILS	27-20 UPDATED WALL DETAILS	DATE REVISION
			204-0	03-	
CLAY CAP AND COMPACTED ON SITE SOIL. BACK FACE MAY BE IRREGULAR FILTER FABRIC AROUND DRAINAGE ZONE, MIRAFI 140N OR APPROVED EQUAL.	DATE BY	DES. 03-12-20 MMR	DRN. 03-12-20 MMR	03-12-20	-
CONTINUOUS GRAVEL OR CLEAN FREE DRAINING ROCK, SEE RUY GENERAL NOTES EXTEND UNDER UPPER WALL AS SHOWN FILTER FABRIC OVER END OF WEEP PIPE COMPACTED SOIL BELOW WEEP PIPE.	Falltafelta Enninaerina Inc	Structural Engineering Consultants	TX Reg. Engineering Firm F-4038	FALKOFSKE	- ONCO-TOZ (/ TO) SUIJENS
	The use of these plans and	specifications shall be restricted to the original site for which they were prepared. Any reproduction or distribution is	expressly limited to such use. Any other reproduction, reuse, or disclosure by any method, in whole, or in port, is prohibited.	These drawings and specifications contain proprietary information and title remains in FALKOFSKE ENGINEERING.	
$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	ONRY RETAINING WALLS BOR HFIGHTS	NWC HARBOR HEIGHTS DRIVE AND SUNSET RIDGE DRIVE ROCKWALL TFXAS		UNY CO DRIZON	TEXAS 75032
TYPICAL WALL SECTION – LOWER TERRACED WALL 1V:8H MAX SLOPE BELOW WALL BEARING IN CLAYEY OR SANDY SOILS		I COMAS J	OF T	μ2 HC . 0 μ2 HC . 0	6 V Winterson

2 RW5







	1500 psf -	BEARING CAP		Y WALL SCH NATURAL UNDIS		s see gener.	L NOTES SHI	SET RW1)	
Wall Height H	BASE WIDTH B	toe B1	BASE DEPTH (TOE) C	BASE DEPTH (HEEL) C1	BATTER A	FULLY MORTARED ZONE E	THICKNESS OF WALL T	DRAINAGE ZONE THICKNESS G	BEARING
1'-0"	1'-0"	0'-0"	1'-0"	0'-2"	0'-2"	FULLY MORTARED	1'-0"	SEE A/RW6	
2'-0"	1'-2"	0'-2"	1'–3"	0'-3"	0'-4"	FULLY MORTARED	1'-0"	SEE A/RW6	
3'-0"	1'-8"	0'-3"	1'-6"	0'-4"	0'-6"	FULLY MORTARED	1 ' -5"	SEE A/RW6	
4'-0"	2'-4"	0'-4"	2'-0"	0'-5"	0'-8"	FULLY MORTARED	2'-0"	SEE A/RW6	1500 p
5'-0"	3'-0"	0'-5"	2'-3"	0'-7"	0'-10"	0'-8"	2'-7"	1'-0"	
6'-0"	3'-8"	0'-7"	2'-6"	0'-8"	1'-0"	0'-10"	3'-1"	1'-0"	
	WALL DESIGN CRITERIA								
BEARING Qa	SLOPE TOP β	SLOPE BOT β1	ACTIVE PRESSURE Фа	PASSIVE PRESSURE Φp	FRICTION ANGLE BASE õ	SLOPE OF BACK OF WALL	SURCHARGE q		
1500PSF	5.71 deg	14 deg	26 deg	26 deg	17 deg	99.46 deg	0 psf	1	

TYPICAL WALL

1 RW6

L	SECTI	ON	_	1V:1	ОН	MAX	SL	OPE	ABO	VE	WALL	
	1V:4H	MA	X :	SLOPI	E BI	ELOW	W	ALL				
E/	ARING	IN	CL	AYEY	OR	SAN	DY	SOIL	S			

				≻					
				BΥ					
				REVISION					
				ΤE					
				NO. DATE					
ВY	20 TJW	20 RL	20 TJW	-					
DATE	S. 04-22-	DRN. 04-22-20	CHK. 04-22-20 TJW	-					
	nts DES		CH						
Eallrafalra Encinación Inc	Structural Engineering Consultants DES. 04-22-20 TJW	TX Reg. Engineering Firm F-4038	Arlington, Texas 76012						
			FALKOFSKE	ENGINEERING					
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MASONRY RETAINING WALLS	NWC HARBOR HEIGHTS DRIVE AND SUNSET RIDGE DRIVE		F.C. CUNY CORPORATION #2 Horizon court suite 500	HEAT, TEXAS 75032					
Interest		WHIT 1895 CENST	8 .	Magini wa					
JO	B N). 7	748.1	9					
	К	VV	0						

 $1/2^{*} = 1'-0^{*}$