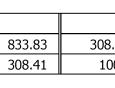
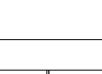
ΡΙ	ΡΕ	ΗY

	COLLECT T (Inlet o anhole)
UPSTREAM STATION	DOWNSTREAM STATION
STA	STA
1	STA 2

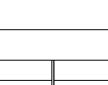
POINT	COLLECTION (Inlet or hhole)	tion Points	INCREMEN		VAGEARE	A	ation	:y (yrs.)	(/hr)	"Q"	dient "S"	xes		r Size	n Collection	ý	pstream	wnstream J	²/2g -	² /4g -		хL	Grade	c Grade	nce / V x 60	Station		
UPSTREAM STATION	DOWNSTREAM STATION	Distance Between Collect	Area No.	Drainage Area	Runoff Coeff. "C"	Accumulated "CA"	Time at Upstream St	Design Storm Frequenc	Intensity "I" (inches	Storm Water Runoff	Slope of Hydraulic Grad	No. of Pipes or Boy		Selected Storm Sewei	Velocity in Sewer Betweer Points "V"	Head loss Coeff. I	Velocity Head Loss at U _I Station V2 ² /2g	Velocity Head Loss at Dov Station KjV1 ² /2g	Velocity Head Loss (V ₂ KV1 ² /2g)	Velocity Head Loss (V ₂ KV1 ² /4g)	Total Velocity Headloss	Friction Loss = Sf	Upstream Hydraulic (Downstream Hydraulic	Flow Time in Sewer Distar	Time of Downstream S	Remarks	
5TA 1	STA 2	ft 3	4	acres 5	6	7	min 8	yrs 9	in/hr 10	cfs 11	ft/ft 12		-	of ft L 3	fps 14	15	ft 16	ft 17	ft 18	ft 19	ft 20	ft 21	ft 22	ft 23	min 24	min 25	26	
							_						HT.	Dia. W														
												S	TM L	(NE 1)	6													
59.74 20.12 16.12	2220.12 2216.12 2037.65 2033.65	39.62 4 178.47	16-K PIPE SIZE 16-J	1.48	0.5 0.5 0.5	0.74 0.74 1.49	10.00 10.16 10.19	100 100 100	9.80 9.73 9.72	7.25 7.20 14.43	0.0048 0.0010 0.0041	1 1 1		18 24 24 27	4.11 2.30 4.60	1.25 0.60 0.60	0.26 0.08 0.33	0.33 0.05 0.20	0.26 (0.25) 0.28		0.263 (0.247) 0.280	0.19 0.00 0.73	514.41 514.47 514.18	514.67 514.22 514.46 513.46	0.16 0.03 0.65	10.16 10.19 10.84	TC=533.10 TC=533.10	Pł Pł Pł Pł
37.65 3.65 8.58 4.58	2033.65 1848.58 1844.58 1779.97	4 185.07 4 64.61	PIPE SIZE 16-I PIPE SIZE STM LINE 19	0.77	0.5 0.5 0.5 0.5	1.49 1.87 1.87 3.15	10.84 10.85 11.55 11.57	100 100 100 100	9.43 9.42 9.11 9.10	14.00 17.61 17.03 28.61	0.0020 0.0032 0.0017 0.0049	1 1 1 1		27 27 30 30	3.53 4.44 3.48 5.84	0.60 0.60 0.60 0.60	0.19 0.31 0.19 0.53	0.12 0.18 0.11 0.32	(0.00) 0.19 0.00 0.42		(0.004) 0.190 0.004 0.418	0.01 0.60 0.01 0.31	513.46 513.26 512.66 512.24	513.45 512.66 512.65 511.92	0.02 0.69 0.02 0.18	10.85 11.55 11.57 11.75	TC=530.05	PI PI PI
79.97 92.68 38.68	1692.68 1688.68 1548.54	87.29 4 140.14	16-H PIPE SIZE 16-G	0.90	0.5 0.5 0.5 0.5	3.60 3.60 3.60 3.93	11.37 11.75 11.97 11.98	100 100 100 100	9.01 9.01 8.92 8.91	32.41 32.05 35.02	0.0062 0.0037 0.0044	1 1 1 1		30 30 33 33	6.62 5.41 5.91	0.60 0.60 0.60	0.68 0.45 0.54	0.41 0.27 0.33	0.12 0.36 0.05 0.27		0.362 0.046 0.270	0.51 0.54 0.01 0.61	511.56 510.97 510.68	511.92 511.01 510.95 510.07	0.10 0.22 0.01 0.40	11.75 11.97 11.98 12.38	TC=527.36 TC=528.28	P P P
18.54 14.59 78.86 91.33	1544.59 1478.86 1391.33 1286.12	3.95 65.73 87.53 105.21	PIPE SIZE STM LINE 18 16-F 16-E	1.44 1.22 0.74	0.5 0.5 0.5 0.5	3.93 4.65 5.26 5.63	12.38 12.39 12.58 12.81	100 100 100 100	8.73 8.73 8.64 8.54	34.32 40.58 45.46 48.09	0.0026 0.0037 0.0046 0.0052	1 1 1 1		36 36 36 36	4.87 5.76 6.45 6.82	0.60 0.60 0.60 0.60	0.37 0.51 0.65 0.72	0.22 0.31 0.39 0.43	0.04 0.29 0.34 0.34		0.042 0.294 0.337 0.335	0.01 0.24 0.41 0.55	510.03 509.72 509.14 508.40	510.02 509.48 508.74 507.85	0.01 0.19 0.23 0.26	12.39 12.58 12.81 13.07	TC=525.95 TC=525.96	P P P
6.12).61 I.35	890.61 884.35 541.5	395.51 6.26 342.85	MH 16-D 16-C	1.70 2.30	0.5 0.5 0.5 0.5	5.63 5.63 6.48 7.63	12.01 13.07 14.05 14.06	100 100 100 100	8.43 7.99 7.98	47.44 51.76 60.89	0.0052 0.0051 0.0060 0.0083	1 1 1 1		36 36 36 36	6.73 7.34 8.64	0.60 0.60 0.60	0.72 0.70 0.84 1.16	0.13 0.42 0.50 0.70	0.31 0.27 0.42 0.66		0.335 0.270 0.415 0.656	2.00 0.04 2.86	507.58 505.17 504.47	507.65 505.58 505.13 501.62	0.98 0.01 0.66	14.05 14.06 14.72	TC=525.82 TC=522.51 TC=522.51	P P P
41.5 5.37 0.88 9.36	535.37 460.88 189.36 100	6.13 74.49 271.52 89.36	16-B 16-A STM LINE 17 & MH A-13	0.31 0.83 1.43 0.60	0.5 0.5 0.5 0.5	7.79 8.20 8.92 9.22	14.72 14.73 14.87 15.34	100 100 100 100	7.68 7.68 7.62 7.41	59.82 62.97 67.91 68.25	0.0080 0.0089 0.0104 0.0105	1 1 1 1		36 36 36 36	8.49 8.93 9.63 9.68	0.60 0.60 0.60 0.60	1.12 1.24 1.44 1.46	0.67 0.74 0.86 0.87	0.42 0.57 0.70 0.59		0.423 0.568 0.697 0.591	0.05 0.66 2.81 0.94	501.19 500.58 499.21 495.81	501.14 499.91 496.40 494.87	0.01 0.14 0.47 0.15	14.73 14.87 15.34 15.50	TC=520.5 TC=520.11 TC=513.11	P P P P
			Subtotal	18.43									Ш	Ш					U	g Hgl IS Ff	ROM STM LI						II.	
												S		(NE 17										502.66				
.83 .41	<u>308.41</u> 100	525.42 208.41	17-B 17-A Subtotal	0.86 0.57 1.43	0.5 0.5	0.43	10.00 13.66	100 100	9.80 8.16	4.21 5.83	0.0016	1		18 18	2.39 3.31	1.25 0.60	0.09 0.17	0.11 0.10	(0.03) 0.06 BEGINNIN	G HGL IS FF	(0.027) 0.059 ROM STM L	0.85 0.64 INE 16 STA	502.69 501.79 : 4+60.88	501.85 501.14 501.14	3.66 1.05	13.66 14.71	TC=525.32 TC=521.85	F
				1	1	1	1		1	1	11 11		STM	16-A	1		1							F00 00				
.51	0	20.51	16-A Subtotal	0.83	0.5	0.42	10.00	100	9.80	4.07	0.0015	1		18	2.31	1.25	0.08	0.10	0.08 BEGINNING I	HGL IS FRO	0.083 M STORM L	0.03 INE 16 ST	499.94 4: 4+02.42	500.02 499.91 499.91	0.15	10.15	TC=520.11	F
													STM	16-B										501.16				
74	0	16.74	16-B Subtotal	0.31	0.5	0.16	10.00	100	9.80	1.52	0.0002	1		18	0.86	1.25	0.01	0.01 EXISTIN	0.01 Ig Hgl Is Fr	ROM EXISTI	0.012 ING STORM	0.00 LINE B ST	501.15 A: 5+16.60	501.14 501.14	0.32	10.32	TC=520.5	F
													STM	16-C										502.47				
.46	0	19.46	16-C Subtotal	2.30 2.30	0.5	1.15	10.00	100	9.80	11.27	0.0115	1		18	6.39	1.25	0.63	0.79 EXISTIN	0.63 G HGL IS FR	ROM EXISTI	0.635 ING STORM	0.22 LINE B ST	501.84 A: 8+86.03	501.62	0.05	10.05	TC=522.51	Р
81	0	16.81	16-D	1.70	0.5	0.85	10.00	100	9.80	8.33	0.0063	1	STM	16-D	4.73	1.25	0.35	0.43	0.35		0.347	0.11	505.24	505.58 505.13	0.06	10.06	TC=522.51	F
			Subtotal	1.70			10,000	100					11	Ш					ig Hgl Is Fr	ROM EXISTI					0100	10100		
													STM	17-A										494.92				
32	0	8.32	17-A Subtotal	0.57 0.57	0.5	0.29	10.00	100	9.80	2.79	0.0007	1		18	1.58	1.25	0.04	0.05 EXISTING	0.04 HGL IS FRO	OM EXISTIN	0.039 IG STORM L	0.01 INE 17 ST	494.88 A: 3+08.41	494.87 494.87	0.09	10.09	TC=513.11	<u> </u>

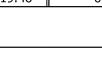


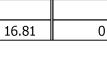












17-A / 17-B

viscol response	tation tation s/hr) s/hr) s/hr) s/hr) s/hr) kj kj kj kj	wnstrean g 2 ² /2g - 2 ² /4g - x L X L Grade ic Grade ic Grade	
1 2 3 4 5 6 7 6 10 11 12 13 10 15 15 17 18 18 20 21 22 1 1 1 1 1 1 10 <t< th=""><th></th><th>Loss a ad Loss a ad Loss ad Loss ad Loss ad Loss a hydra n Hydra ver D ver D ver to</th></t<>		Loss a ad Loss a ad Loss ad Loss ad Loss ad Loss a hydra n Hydra ver D ver D ver to	
Image:			
Table 1 Table 1 <t< td=""><td></td><td></td></t<>			
222.12 232.12 49.0 56.4 1.46 6.5 2.8 1.00 6.30 1 1.8 4.11 1.25 6.25 6.20 6.5 5.4.4 222.12 223.6 233.6 4.6 6.5 2.4.4 3.00 1 2.4 2.33 6.0 0.20 0.227 2.53 6.0 0.25 0.208 0.227 2.53 6.0 0.25 0.208 0.227 2.53 6.0 0.25 0.208 0.227 2.53 6.0 0.25 0.208 0.227 5.54 0.208 6.2 0.33 6.21 0.208 6.23 6.21 0.208 6.23 6.21 0.208 6.23 6.21 0.208 6.23 6.21 0.208 6.23 6.21 0.208 6.23 0.21 0.23 6.21 0.208 6.23 2.20 6.21 2.20 6.21 2.20 6.21 2.20 6.21 2.20 6.21 2.20 6.21 2.20 6.21	STM LINE 16		
1333.05 1980.26 1967.7 1-14 0.07 0.53 0.78 0.16 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.00 0.10 0.00 0.10 0.00 0.10 0.00 0.00 0.10 0.00	4 10.16 100 9.73 7.20 0.0010 1 24 2.30 0.60 0.08 9 10.19 100 9.72 14.43 0.0041 1 24 2.40 0.60 0.33	0.05 (0.25) (0.247) 0.00 514.47 514.46 0.03 10.19 0.20 0.28 0.280 0.73 514.18 513.46 0.65 10.84 T	
19498 179/97 64.0 SNU ME 12 2.55 0.5 3.15 11.57 100 200 28.1 6.000 1.2 20 58.0 6.000 0.33 0.12 0.42 0.418 0.31 52.156 1707.07 1002.00 87.26 164 0.00 0.5 3.00 11.77 100 50.0 20.6 6.00 0.06 0.61 0.35 0.02 0.64 0.51 0.30 0.51 50.02 150.52 1985.66 17385 1997 0.5 3.33 11.38 100 6.73 3.41 20 0.61 1.3 2.77 0.57	7 10.85 100 9.42 17.61 0.0032 1 27 4.44 0.60 0.31	0.18 0.19 0.190 0.60 513.26 512.66 0.69 11.55 T	
Image by Parts H	5 11.57 100 9.10 28.61 0.0049 1 30 5.84 0.60 0.53	0.32 0.42 0.418 0.31 512.24 511.92 0.18 11.75	
144.86 64.73 51M UB-18 1.44 0.5 4.66 12.3 100 8.77 4.08 100 8.77 0.60 0.51 0.31 0.23 0.24 0.24 9.74 9.72 1474.86 1313 67.33 167 1.22 0.5 5.26 12.84 100 8.64 4.564 0.002 1 36 6.47 0.00 0.01 0.33 0.34 0.33 0.24 0.24 0.24 9.72 0.20 0.27 0.20 0.27 0.20 2.00 <t< td=""><td><u>3 11.98 100 8.91 35.02 0.0044 1 33 5.91 0.60 0.54</u></td><td>0.33 0.27 0.270 0.61 510.68 510.07 0.40 12.38 T</td></t<>	<u>3 11.98 100 8.91 35.02 0.0044 1 33 5.91 0.60 0.54</u>	0.33 0.27 0.270 0.61 510.68 510.07 0.40 12.38 T	
1991.33 1981.23 1052.12 1052.11 1052.1 <td>5 12.39 100 8.73 40.58 0.0037 1 36 5.76 0.60 0.51</td> <td>0.31 0.29 0.294 0.24 509.72 509.48 0.19 12.58</td>	5 12.39 100 8.73 40.58 0.0037 1 36 5.76 0.60 0.51	0.31 0.29 0.294 0.24 509.72 509.48 0.19 12.58	
1980.61 884.85 6.76 16-D 1.70 0.55 6.48 140.5 100 7.99 6.78 6.080 1 36 7.24 0.00 0.44 0.50 0.44 0.517 0.517 884.35 515.15 323.25 16.6 2.31 16.5 2.31 16.6 2.31 6.66 0.00 1.13 6.66 0.00 1.14 0.67 0.64 0.63 0.13 0.57 0.42 0.42 0.42 0.43 0.03 0.11 555.37 40.186 7.47 1.05 7.97 14.72 1.00 7.88 6.287 0.0080 1 36 8.49 0.60 1.21 0.67 0.64 0.42 0.42 0.43 0.03 0.03 0.14 0.66 0.60 0.42 0.42 0.43 0.43 0.43 0.43 0.43 0.43 0.43 0.43 0.43 0.43 0.44 0.45 0.44 0.43 0.43 0.43 0.44 0.44 0.45 0.44 0.43 0.43 <th0.43< th=""> 0.44 0.44<!--</td--><td>3 12.81 100 8.54 48.09 0.0052 1 36 6.82 0.60 0.72</td><td>0.43 0.34 0.335 0.55 508.40 507.85 0.26 13.07 T</td></th0.43<>	3 12.81 100 8.54 48.09 0.0052 1 36 6.82 0.60 0.72	0.43 0.34 0.335 0.55 508.40 507.85 0.26 13.07 T	
Sets. 32 6.13 11-B 0.31 0.5 7.79 14.72 100 7.68 6.98.20 0.0080 1 36 8.49 0.60 1.12 0.67 0.42 0.423 0.405 501.19 353.37 490.80 P.173 100 7.68 6.297 0.0080 1 36 8.43 0.60 1.21 0.77 0.427 0.058 0.65 0.50.8 460.88 199.36 271.52 STM LINE 17.8 MH 1.43 0.5 9.22 15.34 100 7.62 67.91 0.0104 1 36 9.63 0.60 1.44 0.66 0.77 0.659 2.61 499.21 1289.36 100 8.0.6 1.5 9.22 15.34 100 7.44 64.25 0.0104 1.44 0.66 0.55 0.54 499.21 1289.30 308.41 592.42 17.78 0.85 0.43 10.00 1.00 8.06 53 0.031 1.8	8 14.05 100 7.99 51.76 0.0060 1 36 7.34 0.60 0.84	0.50 0.42 0.415 0.04 505.17 505.13 0.01 14.06 T	
460.88 129.36 27.52 STM LINE 17.8 MH 1.43 0.5 8.92 1.46 100 7.62 67.91 0.0104 1 36 9.63 0.60 1.44 0.66 0.70 0.697 2.81 499.21 189.36 100 89.30 A.13 0.60 0.5 9.22 15.34 100 7.41 68.25 0.0105 1 36 9.63 0.60 1.44 0.86 0.591 0.95 0.60 0.01 (0.03) (0.027) 0.85 502.69 308.41 100 20.86 0.950 4.07 0.001 1 18 3.31 0.60 0.11 (0.03) (0.027) 0.85 502.69 308.41 100 20.85 16.6 5.83	9 14.72 100 7.68 59.82 0.0080 1 36 8.49 0.60 1.12	0.67 0.42 0.423 0.05 501.19 501.14 0.01 14.73	
STM LINE 1.7 STM LINE 1.7 833.83 308.41 525.42 17.8 0.86 0.5 0.43 100 100 9.80 4.21 0.0016 1 18 2.39 1.25 0.09 0.11 (0.03) (0.027) 0.85 502.69 308.41 100 208.41 17.4 0.57 0.5 0.72 13.66 100 8.16 5.83 0.0031 1 18 3.31 0.60 0.17 0.10 0.06 0.059 0.64 501.79 Subtolal 1.43 Subtolal 1.43 Subtolal 0.06 0.01 0.06 0.01 0.06 0.06 0.01 0.06 0.01 0.06 0.01 0.00 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 <	2 14.87 100 7.62 67.91 0.0104 1 36 9.63 0.60 1.44	0.86 0.70 0.697 2.81 499.21 496.40 0.47 15.34	
No. No. <td>CTM LINE 17</td> <td>BEGINNING HGL IS FROM STM LINE 15 STA: 8+15.63 494.87</td>	CTM LINE 17	BEGINNING HGL IS FROM STM LINE 15 STA: 8+15.63 494.87	
308.41 100 208.41 17-A 0.57 0.5 0.72 13.66 100 8.16 5.83 0.0031 1 18 3.31 0.60 0.17 0.10 0.00 0.059 0.64 501.79 Subtolal 1.43 Subtolal 1.43 <td></td> <td>0.11 (0.03) (0.027) 0.85 502.69 501.85 3.66 13.66 T</td>		0.11 (0.03) (0.027) 0.85 502.69 501.85 3.66 13.66 T	
STM 16-A 0 0 0.6 0.83 0.5 0.42 1.00 100 9.80 4.07 0.015 1 18 2.31 1.25 0.08 0.10 0.08 0.03 499.94 STM 16-A SUbtotal 0.83 0.5 0.42 10.00 100 9.80 4.07 0.015 1 18 2.31 1.25 0.08 0.10 0.08 0.083 0.03 499.94 STM 16-B STM 16-B 16.74 0 16.74 16-B 0.31 0.5 0.16 10.00 100 9.80 1.52 0.002 1 18 0.86 1.25 0.01 0.01 0.012 0.00 501.15 STM 16-B SUBTORI IDE FROM EXESTING STORM LINE B STA: Stillow STM 16-C STM 16-C STM 16-C STM 16-C STM 16-C <td></td> <td>0.10 0.06 0.059 0.64 501.79 501.14 1.05 14.71 T</td>		0.10 0.06 0.059 0.64 501.79 501.14 1.05 14.71 T	
Image: Normal State Sta	STM 16-A		
STM 16-B 16.74 0 16.74 16-B 0.31 0.5 0.16 10.00 100 9.80 1.52 0.002 1 18 0.86 1.25 0.01 0.01 0.01 0.012 0.00 501.15 Subtoal 0.31 0.5 0.16 10.00 100 9.80 1.52 0.002 1 18 0.86 1.25 0.01 0.01 0.01 0.012 0.00 501.15 0 Subtoal O.31 O.50 O.60 Subtoal O.61 O.60 SUBTOAL COLSPANE XEVENUE B STA: 5+16.60 Subtoal O.31 O.50 O.60 SUBTOAL COLSPANE XEVENUE B STA: 5+16.60 Subtoal O.31 O.60 SUBTOAL COLSPANE XEVENUE B STA: 5+16.60 Subtoal O.61 O.61 O.61 O.61 O.61 O.61 O.61 O.61 O.61 <th colspa<="" td=""><td></td><td>0.10 0.08 0.083 0.03 499.94 499.91 0.15 10.15 T</td></th>	<td></td> <td>0.10 0.08 0.083 0.03 499.94 499.91 0.15 10.15 T</td>		0.10 0.08 0.083 0.03 499.94 499.91 0.15 10.15 T
Image: Normal and the stress of the stres		BEGINNING HGL IS FROM STORM LINE 16 STA: 4+02.42 499.91	
Subtotal 0.31 EXISTING HGL IS FROM EXISTING STORM LINE B STA: 5+16.60 STM 16-C State State State State 19.46 0 19.46 16-C 2.30 0.5 1.15 10.00 100 9.80 11.27 0.0115 1 18 6.39 1.25 0.63 0.79 0.63 0.635 0.22 501.84 0			
Image: Second		0.01 0.01 0.012 0.00 501.15 501.14 0.32 10.32 1 EXISTING HGL IS FROM EXISTING STORM LINE B STA: 5+16.60 501.14 50	
19.46 0 19.46 16-C 2.30 0.5 1.15 10.00 100 9.80 11.27 0.0115 1 18 6.39 1.25 0.63 0.79 0.63 0.635 0.22 501.84	STM 16-C	502.47	
	5 10.00 100 9.80 11.27 0.0115 1 18 6.39 1.25 0.63	0.79 0.63 0.635 0.22 501.84 501.62 0.05 10.05 T EXISTING HGL IS FROM EXISTING STORM LINE B STA: 8+86.03	
STM 16-D	STM 16-D		
16.81 0 16.90 1.70 0.5 0.85 10.00 100 9.80 8.33 0.0063 1 18 4.73 1.25 0.35 0.43 0.347 0.11 505.24	Image: 10.00 Image: 10.00<	0.43 0.35 0.347 0.11 505.24 505.13 0.06 10.06 T EXISTING HGL IS FROM EXISTING STORM LINE B STA: 8+90.61 505.13 50	
	STM 17-A		
8.32 0 8.32 17-A 0.57 0.5 0.29 10.00 100 9.80 2.79 0.0007 1 18 1.58 1.25 0.04 0.05 0.04 0.039 0.01 494.88	9 10.00 100 9.80 2.79 0.0007 1 18 1.58 1.25 0.04	0.05 0.04 0.039 0.01 494.88 494.87 0.09 10.09 T EXISTING HGL IS FROM EXISTING STORM LINE 17 STA: 3+08.41 494.87	

Drainage Area	Area (Acres)	Runoff Coeff.	1.22	Time (conc.) (minutes)	Discharge (c.f.s.)	Comment
	"A"	"C"	" "	T _c	"Q"	
	•			PHASE 7D	DRAINAGE A	REAS
STORM LINE 16						
16-A	0.83	0.5	9.80	10.0	4.07	Developed - Single Family - Phase 7D
16-B	0.31	0.5	9.80	10.0	1.52	Developed - Single Family - Phase 7D
16-C	2.30	0.5	9.80	10.0	11.27	Developed - Single Family - Phase 7D
16-D	1.70	0.5	9.80	10.0	8.33	Developed - Single Family - Phase 7D
16-E	0.74	0.5	9.80	10.0	3.63	Developed - Single Family - Phase 7B
					28.81	
STORM LINE 17						
17-A	0.57	0.5	9.80	10.0	2.79	Developed - Single Family - Phase 7D
17-B	0.86	0.5	9.80	10.0	4.21	Developed - Single Family - Phase 7D
				1	7.01	

			RUI	NOFF CALC		IS PHASE 7D
Drainage Area	Area (Acres)	Runoff Coeff.	Intensity (in./hr.)	Time (conc.) (minutes)	Discharge (c.f.s.)	Comment
	"A"	"C"	"l"	T _c	"Q"	
				OFFSITE	DRAINAGE	AREAS
STORM LINE B						
B-1	2.14	0.5	9.80	10.0	10.49	Developed - Single Family - Phase 8B
B-2	2.74	0.5	9.80	10.0	13.43	Developed - Single Family - Phase 8B
B-4	3.50	0.5	9.80	10.0	17.15	Developed - Single Family - Phase 8B
B-5	0.47	0.5	9.80	10.0	2.30	Developed - Single Family - Phase 8B
					43.37	
STORM LINE 16						
16-F	1.22	0.5	9.80	10.0	5.98	Developed - Single Family - Phase 7B
16-G	0.67	0.5	9.80	10.0	3.28	Developed - Single Family - Phase 7B
16-H	0.90	0.5	9.80	10.0	4.41	Developed - Single Family - Phase 7B
16-I	0.77	0.5	9.80	10.0	3.77	Developed - Single Family - Phase 7B
16-J	1.49	0.5	9.80	10.0	7.30	Developed - Single Family - Phase 7B
16-K	1.48	0.5	9.80	10.0	7.25	Developed - Single Family - Phase 7B
					32.00	· · · ·
STORM LINE 18						
18-A	0.51	0.5	9.80	10.0	2.50	Developed - Single Family - Phase 7B
18-B	0.93	0.5	9.80	10.0	4.56	Developed - Single Family - Phase 7B
					7.06	
STORM LINE 19						
19-A	1.10	0.5	9.80	10.0	5.39	Developed - Single Family - Phase 7B
19-B	1.45	0.5	9.80	10.0	7.11	Developed - Single Family - Phase 7B

BENCHMARKS	
 X-chiseled in CL of Alley East of Morningstar Drive within the third lot north of Midnight Pass. 	
Elevation = 513.26	
2. PK Nail in CL of Caruth Lane & Alley intersection	
150 feet +/- east of Morningstar Drive.	

100 10 9.80 0.5 0.83 4.07

100 10 9.80 0.5 2.30 11.27

100 10 9.80 0.5 0.74 3.63

10 9.80 0.5 0.57 2.79

0.5 0.31 1.52

0.5 1.70 8.33

9.80

9.80

17-B 100 10 9.80 0.5 0.86 4.21

NO.	REVISIONS DURING CONSTRUCTION	BY	DAT

1.4

ings Elevation = 491.68

16-A

16-B

16-C

16-D

17-A

16-E

100

100

100

10

10

NOTE: INLET 17-A OVERFLOW WILL BE CAPTURED AT INLET 14-A CONSTRUCTED WITH CARUTH LAKES PHASE 7C.

16-A

16-B

16-C

16-D

16-E

17-A

17-B

STORM LINE 16

STORM LINE 17

19+68.74 CRESCENT COVE DRIVE

18+54.59 CRESCENT COVE DRIVE

14+80.46 CRESCENT COVE DRIVE

14+80.46 CRESCENT COVE DRIVE

13+29.63 ALLEY 6 NORTH

2+09.97 ALLEY 6 NORTH

7+27.61 ALLEY 6 NORTH

4.07	21.00	0.94	6" PARABOLIC	10	5.80	-	4.07
1.52	18.00	0.60	6" PARABOLIC	10	5.80	-	1.52
11.27	-	-	SAG	10	20.00	-	11.27
8.33	-	-	SAG	5	10.00	-	8.33
3.63	26.50	1.43	5" INVERT	10	6.25	-	3.63
4.21	18.50	0.69	5" INVERT	5	2.80	1.41	2.80
4.21	18.50	0.69	5" INVERT	5	2.80	1.41	2.80

04-13-2015

DATE

AS-BUILT DRAWING TO THE BEST OF JBI PARTNERS, INC. KNOWLEDGE HEREBY STATES THIS PLAN IS AS-BUILT. THE INFORMATION PROVIDED IS BASED ON CONSTRUCTION STAKING AND PAD VERIFICATION AT THE SITE AND INFORMATION PROVIDED BY THE CONTRACTOR.



The seal appearing on this document was authorized by DANIEL DEWEY, P.E. 93961. Alteration of a sealed document without proper notification to the responsible engineer is an offense under the Texas Engineering Practice Act.





ALL RESPONSIBILITY FOR ADEQUACY OF DESIGN REMAINS WITH THE DESIGN ENGINEER. THE CITY OF ROCKWALL, IN REVIEWING AND RELEASING PLANS FOR CONSTRUCTION, ASSUMES NO RESPONSIBILITY FOR ADEQUACY OR ACCURACY OF DESIGN.

	DRAINAGE CALCULATIONS	PROJECT NO.
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Main 972.248.7676 Fax 972.248.1414 www.jbipartners.com	Caruth Lakes Phase 7D	SHEET NO.
	City of Rockwall, Texas	11