

REVISION SEP 1 4 2021

CITY OF ROCKWALL ENGINEERING DEPT.

GENERAL NOTES

1. Design

1.1. Design Codes

International Building Code, 2015 Edition

1.2. Geotechnical Report

rm: RONE ENGINEERING, Inc. eport No. 16-21084 Dated: May 12, 2016

1.3. Design Parameters

Soil Parameters

Soil Type*	Friction Angle	Cohesion (psf)	Unit Weight (pcf)
Retained Backfill (On site clay)	26 deg	0 psf	120 pcf
Foundation Soils (1500 psf)	26 deg	0 psf	120 pcf

*See materials below for a description of each Soil Type

Factors of Safety:

External Stability
a. Minimum Factor of Safety Against Base Sliding (Static Condition)
b. Minimum Factor of Safety Against Overturning
c. Minimum Factor of Safety Against Global Stability
d. Minimum Factor of Safety For

Design Loading:

Lateral earth pressures are calculated using Coulombs Lateral Earth Pressure Theory. Designs have been performed to accept loading per the proposed loading conditions based on the Civil Grading Plans. A live loading of 250 psf has been used for all walls supporting areas subject to frelane loading.

Retaining walls should not have solid fence (such as wood fence) placed on top of well other than that shown on these plans. Retaining walls shall not have additional surcharge placed above wall other than that shown on these plans. Retaining walls shall not have slope at base or top of wall that exceed that within is shown on these plans. The retaining walls noted above require special design.

2. Materials

2.1. Soil Types

- a. Retained Backfill
- a.a. On site clayey soils
 a.b. Properly compacted on-site fill soils, verification by others.

- b. Foundation Soils (Allowable Bearing = 1500 pef min)
 b.a. Bearing on Stiff Natural Undisturbed Clayey or Sandy Soils or Compacted and Tested Fill Soils
 b. Friction Angle between Base of Wall and Soil 17 deg
 b. Bearing in fill soils. Fill soils supporting the retaining walls shall be placed in accordance with the recommendations for the fill placement per the geotechnical report.
- . Drainage Material c.a. Free draining granular backfill, clean, non-plastic, relatively well-graded.

- 2.2. Dimension Stone
 a. Average Density of masonry wall varies from 135pcf to 145pcf.
 b. Stone size varies from 4" to 18".
 c. Face stone shall be coordinated between contractor and owner/developer.
 d. Recycled concrete 4" to 18" may be used in place of dimension stone, contractors option.

2.3. Rebar/Welded Wire Fabric (If Required)

- All steel reinforcement shall be new billet steel conforming to ASTM A-615, Grade 60 with fy=60kai. All reinforcement shall not have deleterious material on it.
 All welded wire fabric shall have minimum fy=65ksi and be hot dip galvanized.

2.4. Drainage Materials

- Weep pipes shall be PVC or corrugated HDPE pipe.
 Drainage zone shall be separated from retained backfilt by mirafi 140N filter fabric or approved equal.

2.5 Portland Cement Mortar for Retaining Wall Construction.

The portland cement mortar used for construction of the masonry stone retaining walls shall be provided with the following proportions per cubic yard of concrete. The portland cement mortar supplier shall provide "batch lickels" clearly indicating that the appropriate amount of materials are provided in each truck load. The batch lickels shall clearly indicate the amount batched, the date, the project name and shall be provided to Falkofske Engineering, Inc. for review, documentation, and file.

Contents	Amount per cubic yard	Specific Gravity	Volume ft^3
Type 1 Portland cement:	451 lbs	3.15	2.29
Type F Fly Ash	113 lbs	2.93	0.62
Fine Aggregate (sand):	2746 lbs	2.59	16.99
Potable Water	367 lbs	44 Gallons	5.88
Sika Air (or equivalent)	(AS REQ'D) oz	4.5%	1.22 27.0 Total

Note: the portland cement mortar supplier material weights may vary slightly based on the specific gravity of the materials used.

Concrete retarders may be used at the discretion of the masonry wall contractor. A greater amount of retarder is typically used during hot periods and a less amount of retarder is typically used during cool weather.

3. Construction

3.1 Preparation Work

- Prior to grading or excavation of the site, confirm the location of the retaining walls and all underground features, including utility location within the area of construction. Ensure surrounding structures are protected from effects of wall excavation, and construction.
 Coordinate installation of underground utilities and other improvements with wall installation.

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- a. If a mortared footing is over-excavated, then the dimension stone shall be placed mortared. If a dry stone footing is over excavated, then the dimension stone does not need to be mortared. It is the place of the state of the wall construction exceeds 4 feet in height.
 c. In areas where the wells are notated in a cut. the required excavation shall extend horizontally to the extent of the wild hort of the retaining wall. The wall may be built to the cut. If the wall is over cut, then so shall either be compacted or the drainage zone may be widened.

- The wall shall be constructed to the dimensions as shown on these plans. Front leads, back leads, and string lines shall be set for each wall. Care shall be taken to install the mortar zones the correct thickness, and to place drainage behind the wall as required.
 Control joints shall be installed at a maximum of 16-0" o.c. per these plans.
 Weep pipes shall be placed at 5-0" o.c. max.
 Asor rock type shall be controlled between the architect, owner, and retaining wall contractor.

3.4 Retained Backfill Placement

- Retained backfill shall be placed per the recommendations of the geotechnical engineer, but should not be less than 93% Standard Proctor Maximum Dry Density (ASTM D599).
 Fill should be placed in maximum 8" thick compacted lifts.
 Large compaction equipment (equipment heavier than 7.500 tb) shall remain a minimum of 1.5x the height of the wall dava prior the vall for a period of 2 weeks from the time of
- construction.

 After a period of 2 weeks from the time of construction large compaction equipment may be used behind the wall but shall stay a minimum of 5-0° away from the back of the wall.

 Soil placed with in 5-0° of the back of the wall shall be placed using handheld compaction
- equipment.

 If the wall is in a cut situation the wall may be built up to the cut. If the wall is overcut the drainage zone may be widened to the cut or compacted fill may be placed between the drainage zone and the cut.

3.6 Retaining Wall Performance, Maintenance, and Other Comments

- Control joints are provided in the retaining wall to allow for minor movements due to settlement and shrink swell of the soils. Some cracking may occur in the face of the retaining wall. This cracking, if minor (less than 36°), may be cosmetically repaired as desired.

 b. The retaining walls are designed to allow surface water to flow over the tops of the retaining walls. Care should be taken during and after construction to not allow water to pond behind the retaining walls, as this can have a negative impact on the stability of the retaining walls.

 c. If downspouts are located near the back of the retaining wall they should either be plumbed through the retaining walls.

 d. Postive draining wall to drain below the wall or collected and tied into the storm sever system. Perforated subsurface pipes shall not be used behind the retaining walls.

 d. Positive drainage over the top of the walls shall be maintained throughout the life of the structure. If swales are placed behind the wall they shall remain clean and free draining. If water is found to be ponding in the swale it shall be fixed to allow water to feely drain as soon as a possible.

 e. Any broken spiriklers behind the retaining wall shall be turned off and repaired as soon as possible.

3.7 Cold Weather Construction of Retaining Walls

Construction Requirements for temperatures between 40°F and 32°F

- a. Water and aggregates used in mortar shall not be heated above 140°F.
 b. Mortar sand or mixing water shall be heated to produce mortar temperatures between 40°F and 120°F at the time of mixing.

onstruction Requirements for temperatures between 32°F and 25°F:

- The guidelines above for construction requirements for temperatures between 40°F and 32°F and the following shall be met.
 The mortar temperature shall be maintained above freezing until used in masonry stone retaining wall.
- wall.

 V. Visible ice and snow shall be removed from the top surface of existing foundations and masonry to receive new construction. These surfaces shall be heated to above freezing, using methods that do not result in damage.

 d. Newly constructed masonry shall be completely covered with weather-resistive membrane for 48

onstruction Requirements for temperatures between 25°F and 20°F.

- a. The guidelines above for construction requirements for temperatures between 40°F and 32°F, the construction guidelines for temperatures between 32°F and 25°F, and the following shall be met.
 b. Masonny (raw stone) surfaces under construction shall be heated to 40°F.
 c. Wind breaks or enclosures shall be provided when the wind velocity exceeds 15 miles per hour.
 d. Newly constructed masonry shall be completely covered with weather-resistive insulating blankets, or equal protection, for 48 hours after being completed.

The above procedures comes from sections 2104.3.2.1, 2104.3.2.2, 2104.3.2.3, 2104.3.3.3, and 2104.3.3.4 of the International Building Code, and is in compliance with Masonry Standards Joint Committee recommendations for cold weather construction of masonry structures.

4. Construction Observations

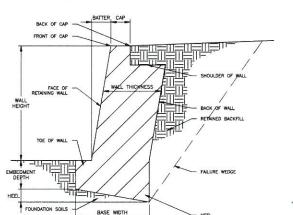
4.1 Construction Observations by Falkofske Engineering, Inc.

- a. Falkofske Engineering, Inc. will perform construction observation, but only as a means of verification of the contractors quality control performance.
 b. Falkofske Engineering, Inc. will act as the Special Inspector for this project. Contractor shall contact Falkofske Engineering to set up inspections, at least 1 day before construction starts.
 c. All required materials testing shall be performed by an approved materials testing laborators.
- (a) A Falkofske Engineering, inc. is not responsible for means, methods, and material furnished by the retaining wall contractor.

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4.2 Construction Observations by Others

a. Construction observations as required by the city shall be coordinated by the contractor.



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Engineering, Ir Engineering Cc Engineering Firr Fielder Road Texas 76012 -8300

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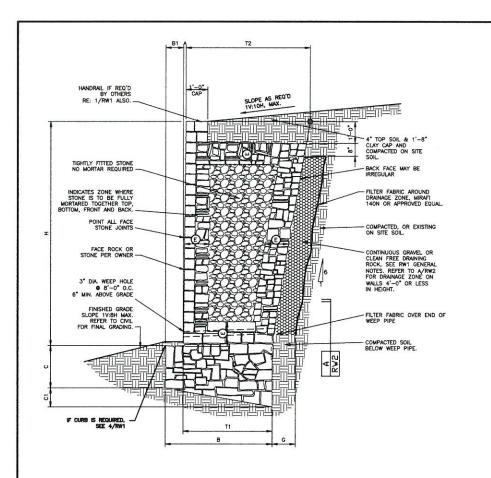
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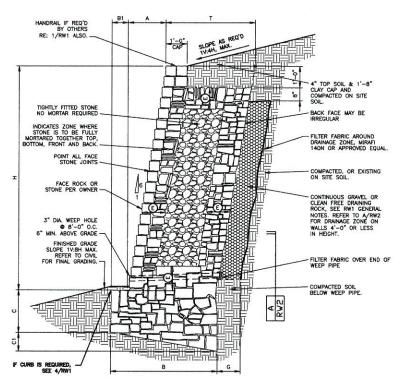
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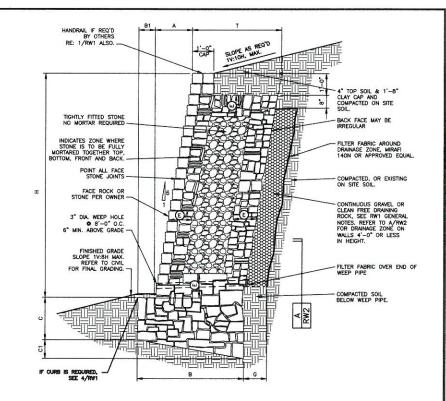
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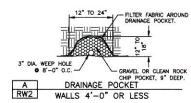
JOB NO. 151.20 8/19/2

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12" TO 24" FILTER FABRIC AROUND DRAINAGE POCKET.	
P.,	
3" DIA WEEP HOLE 8"-0" O.C. GRAVEL OR CLEAN ROCK	
A DRAINAGE POCKET, 9" DEEP. RW2 WALLS 4'-D" OR LESS	

HEROHT H	BASE WIDTH B	TOE B1	DEPTH (TOE) C	DEPTH (HEEL)	BATTER	MQ E	OF WALL	OF WALL T2	DRABNAGE ZONE THICHDRESS G	CAPACITY			
1'-0"	1'-0'300	0'-0"	0'-6" 0	58 0'-2"	1/4"	HORTAGED	1'-0'108	1'-2"	SEE A/RW2				
2'-0"	1'-2" 59	0'-2"	0'-9" 0	92 0'-3"	1/2"	MONTANZO	1'-0" 55	1"-4"	SEE A/RW2				
3'-0"	1'-8" BO	0'-3"	0'-9" 0	92 0'-4"	3/4"	MONTANED	1'-3" 5.0	1'-9"	SEE A/RW2	1500 paf			
4'-0"	2"-1" 52	0'-5"	1'-0" 1	25 0'-5°	1"	MORTANED	1'-8" 50	2'-4"	SEE A/RW2				
5'-0"	2'-9" 55	0'-7"	1'-3" 1	50 0'-6"	0'-1 1/4"	0'-8"	2'-2" 52	3'-0"	1'-0"				
6'-0"	3'-5" 57	0'-10"	1'-6" 1.	83 0'-8"	0'-1 1/2"	0'-10"	2'-7" 52	3'-7"	1'-0"				
7'-0"	4'-0" 58	1"-0"	1'-9" 2.	17 0'-9"	0'-1 3/4"	0'-10"	3'-0" 52	4'-2"	1'-0"				
8'-0"	4'~10"61	1'-4"	2'-3" 2	750'-11"	0'-2"	1'-0"	3'-6" 53	4'-10"	1'-0"				
		WAL	L DESIGN C	RITERIA									
EXAMPLE Qu	SLOPE TOP	SLOPE BOT	ACTIVE PRESSURE	PASSIVE PRESSURE 4p	PRICTION ANGLE BASE	SLOPE OF BACK OF WALL	SURCHARGE q						
1500PSF	5.71 deg	7.13 deg	26 deg	26 deg	17 deg	99.46 deg	0 per						

HEIGHT H	BASE WIDTH B	TOE B1	DEPTH (TOE)	BASE BEFTH (NEEL) C1	BATTER A	The state of the s	THICHESS OF WALL	DRANAGE ZONE THEORNESS G	CAPACITY
1'-0"	1'-0'300	0'-0"	0'-6"	58 0'-2"	0'-2"	MORRANGED	1'-0"	1'-0"	
2'-0"	1'-4" 69	0'-2"	0'-9"	92 0'-3°	0'-4"	MORIDATED	1'-2" 5	1'-0"	
3'-0"	1'-9" 59	0'-3"	0'-9" 0	92 0'-4"	0,-6.	MORTANED	1'-6" 50	1'-0"	
4'-0"	2'-7" 55	0'-4"	1'-0" 1	250'-6"	0'-8"	MORRANGO	2'-3" 51	1'-0"	1500 ps
5'-0"	3'-3" 65	0'-5"	1'-3"	58 0'-7"	0'-10"	0'-8"	2'-10"=	1'-0"	
6'-0"	4'-0" 67	0'-7"	1'-6"	92 0'-9"	1'-0"	0'-10"	3'-5" 51	1'-0"	
7'-0"	4'-10°65	0,-8.	1'-9" :	10'-10"	1'-2"	0'-10"	4'-1" 55	1'-0"	
8'-0"	5'-6" >1	0'-10"	2'-3" 2	751'-0"	1'-4"	1'-0"	4'-10" 61	1'-0"	
9,-0,	6"-10" 76	0'-11"	2'-6"	271'-3"	1'-6"	1'-0"	5'-11" 64	1'-0"	
10'-0"	7'-7" 76	1'-0"	3'-0" 3	75 1'-5"	1'-8"	1'-2"	6'-7" 61	1'-0"	1700 p
11'-0"	8'-5" 76	1'+1"	3'-6" 4	25 1 -6"	1'-10"	1'-2"	7'-4" 6	1'-0"	1900 p
		WAL	L DESIGN C	RITERIA				No. of Control of Cont	
DEADURA DE	SLOPE TOP	SLOPE BOT	ACTIVE PRESSURE	PASSIVE PRESSURE Oc	PRICTION ANGLE BASE	SLOPE OF BACK OF WALL	SURCHARSE		
1500PSF	14 deg	7.13 deg	26 deg	26 dsg	17 deg	99.46 deg	0 psf		

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CITY OF ROCKWALL ENGINEERING DEPT.

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CAPACITY	THICHOLESS G	DECIDEESS OF WALL	ud E	BATTER	BASE DEPTH (HEEL) C1	DEPTH (TOE)	70E 81	BASE WIOTH B	HEIGHT			
	SEE A/RW2	1'-0", 50	MONTHUE	0'-2"	58 0'-2"	0'-6"	0'-0"	1'-0'100	1'-0"			
	SEE A/RW2	1'-0" 30	MOHINED	0'-4"	0'-3"	0'-9"	0'-2"	1'-2" 59	2'-0"			
1500 pef	SEE A/RW2	1'-4" 45	MONTANCO	0'-6"	92 0'-4"	0'-9" 1	0'-3"	11-7" 53	3'-0"			
	SEE A/RW2	1-11-40	MORTANED	0'-8"	250'-5"	1'-0"	0'-4"	2'-3° 57	4'-0°			
	1'-0"	2'-4" 47	0'-8"	0'-10"	500'-6"	1'-3"	0'-5"	2'-9" 55	5'-0"			
	1'-0"	2'-10"	0'-10°	1'-0"	83.0'-8"	1'-6"	0'-7"	3'-5" =7	6'-0"			
	1'-0"	3'-4"	0'-10"	1'-2"	170'-9"	1'-9"	0'-9"	4'-1" 59	7'-0"			
	1'-0"	4'-0" 50	1'-0"	1'-4"	750'-11"	2'-3" 2	0'-11"	4'-11"=2	8'-0"			
	1'-0"	4'-10" 54	1'-0"	1'-6"	081'-1"	2'-6"	1'-1"	5'-11"66	8'~0°			
1600 ps	1'-0"	5'-5° 55	1'-2"	1'-8"	581'-2"	3,-0,	1'-3"	6'-8"	10'-0°			
1700 psf	1'-5"	6'-0" 55	1'-2"	1'-10"	331-4	3'-6"	1'-4"	7'-4" 67	11'-0"			
					UTERIA	DESIGN CI	WALL					
		SURCHARGE	SLOPE OF BACK OF WALL	FRICTION ANGLE BASE	PASSIVE PRESSURE	ACTIVE PRESSURE	SLOPE BOT	SLOPE TOP	SEARING CO			
		0 psf	99,46 dea	17 deg	26 dea	26 deg	7.13 deg	5.71 deg	500PSF			

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AARON M. BERKES

S.E. LOO WORTH

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Falkofske Engineering, Inc. Structural Engineering Consu Texas Registration F-4038 722 North Fielder Road Arlington, Texas 76012 (817) 261-8300

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JOB NO. 151.20

TYPICAL VERTICAL WALL SECTION - 1V:10H MAX SLOPE ABOVE WALL BEARING IN CLAYEY OR SANDY SOILS

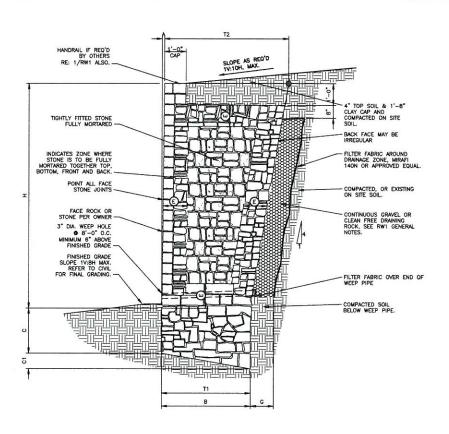
RW2

MAX. SLOPE ABOVE WALL 1V:4H MAX. SLOPE BELOW WALL 1V:8H

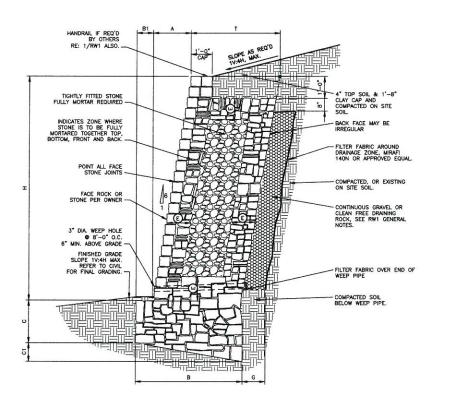
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TYPICAL WALL SECTION - 1V:10H MAX SLOPE ABOVE WALL

1V:8H MAX SLOPE BELOW WALL BEARING IN CLAYEY OR SANDY SOILS



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WALL HEIGHT	BASE WEDTH B	DEPTH (FOE)	DEPTH (HEEL) C1	BATTER A	MOZE E	THEOLOGESS OF VINLL TI	OF WALL T2	THORNES ZONE THORNESS G	CAPACITY
4'-0"	2'-0" 50	1'-0" 1.	25 0'-5°	0'-1"	MONTHERD	2'-0" 63	3'-0"	1"-0"	
5'-0"	2'-8" 50	1'-3" 1.	50 0'-8"	0'-1 1/4"	MONTHEED	2"-6" 64	3'-9"	1"-0"	1500 per 1850 per
80.	3'-0" 50	1'-6" 1.	83 0'-7"	0'-1 1/2"	MOKINGED	3'-0" 63	4'~6"	1'-0"	1850 pef
7'0"	3'-6" 50	1'-9" 2.	08 0'-8"	0'-1 1/2"	MONTH COM	3'-6" 63	5'-3"	1"-0"	2150 per
		WAL	DESIGN C	RIYERIA	2 UH		100		
Ge Ge	SLOPE TOP	SLOPE BOT	ACTIVE PRESEURE bs	PRESSIVE PRESSURE 40	FRICTION ANGLE DASE	SYCK OF MATT	SURCHARGE q		
1500PSF	5.71 deg	7.13 deg	26 deg	26 deg	17 deg	104.04 deg	0 pef	1	



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HEIGHT	BASE WICTH B	TOE B1	BASE DEPTH (TOE) C	BASE DEPTH (HEXX.) C1	BAITER	FULLY MOSTARED ZONE E	THICHONESS OF WALL T	DRAMAGE ZONE THICKNESS G	CAPACIT	
5'-0"	3'-6"	0'-5"	3,-0,	0'-8"	0'-10"	0'-9"	3'-1"	1'-0"		
6'-0"	4'-3" 71	0'-5"	3'-6"	0'-9"	1'-0"	1'-0"	3'-9"	1'-0"	1500 par	
7'~0"	5'-2"	0'-7"	4'-0"	s=0'-11"	1'-2"	1'0"	4'-7"	1'-0"		
8'-0"	6'-1"	0'-8"	4'-6"	28 1'-1"	1'-4"	1'-3"	5'-5"	1'-0"		
8,-0,	7'-3"	0'-9"	5'-0"	171'-3"	1'-6"	1'-3"	6'-6"	1'-0"	CS VALUE	
10'-0"	8'-1"	0'-10"	5'-0"	1'-8"	1'-8"	1'-6"	7'-3"	1'-0"	2000 p	
11'-0"	8,-0,	1'-0"	7'-0"	1'-7"	1'-10"	1'-6"	8'-0"	1'0"		
	WALL DESIGN CRITERIA									
BEATING On	AMEN SLOPE TOP SLOPE BOT PRESSURE PRESSURE PRESSURE AMELE BASE BACK OF WALL SLAPCHARDE									
1500psf	14 deg	14 deg	26 deg	26 deg	17 deg	99.46 deg	Q psf	The state of		

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TYPICAL WALL SECTION - 1V-4H MAX SLOPE ABOVE WALL

1V-4H MAX SLOPE BELOW WALL

BEARING IN CLAYEY SOILS



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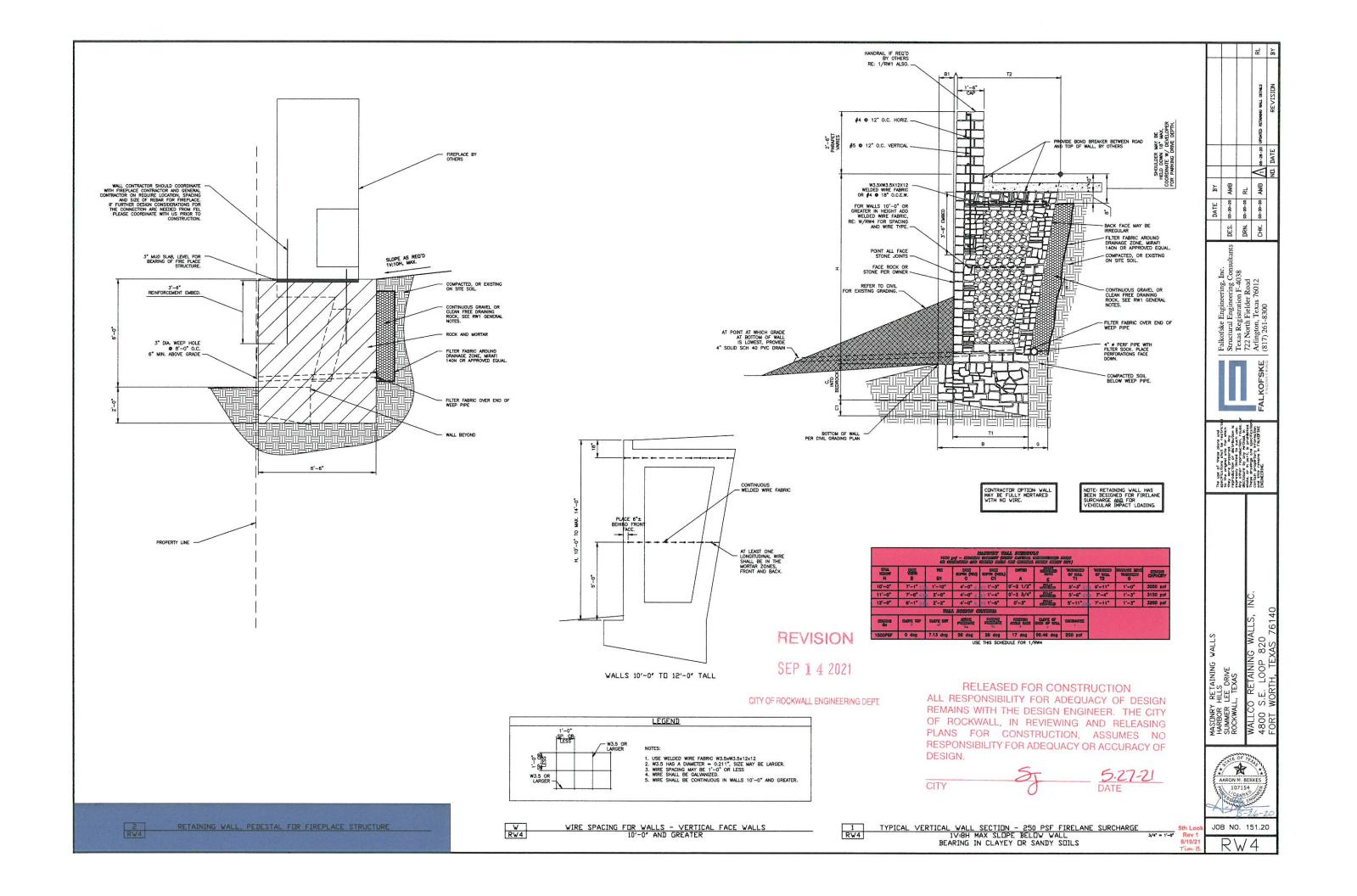
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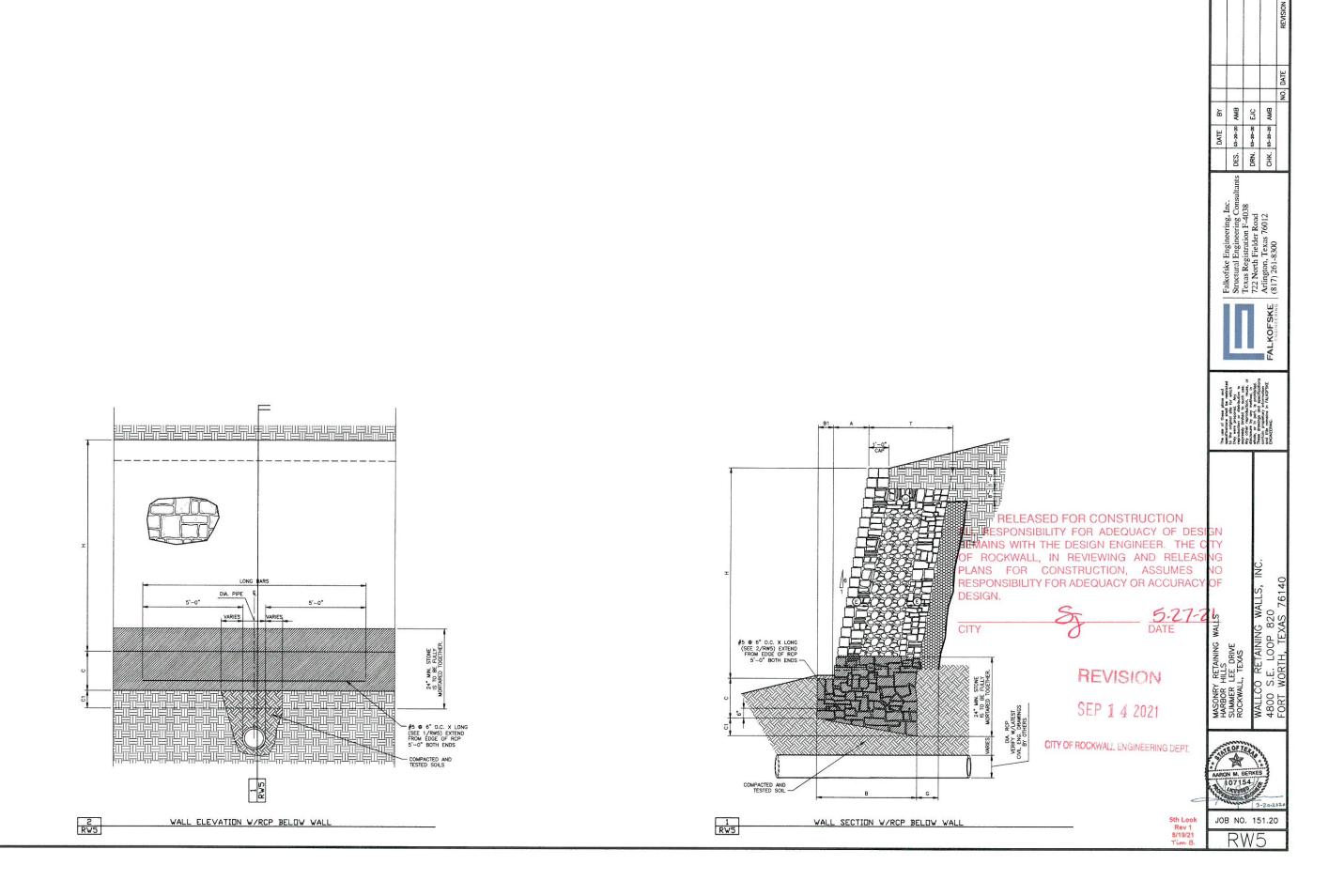
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RW3

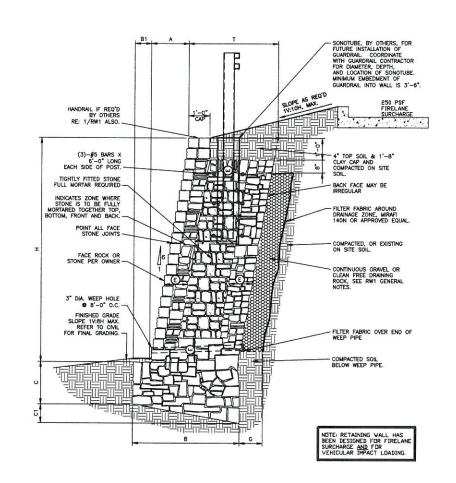
BEARING IN CLAYEY OR SANDY SOILS

3/4" = 1"-0"

5th Look Rev 1 8/19/21 Tim B.







CAPACITY	MECONET ZONE	OF WILL T	E	DAITER A	DEPTH (HEEL) C1	DEPTH (TOE) C	10Z B1	B B	H HSISHL WATT
	1'-0"	3'-9" 63	PERSONAL PROPERTY.	1'-0"	so 1'-0"	2'-0' 2.	1'-6"	5'-3" BB	6'-0"
No.	1'-0"	4'-1" 55	MONHAMO	1'-2"	58 1'-1"	2'-0" 2	1'-6°	5'-7" BO	7'-0°
1500 psf	1'-0"	4'-11"57		1'-4"	58 1'-2"	2'-0" 2.	1'-6"	6'-4" 80	6'-0°
	1'-0"	5'-6" 62	RECEIPTED TO	1'-6"	92 1'-3"	2'-3" 2.	1'-6"	7'-0" 78	9'-0"
1800 psf	1'-0"	6'-0" 60	HOWARD N	1'-8"	17 1'-4"	2'-6" 3	1'-6"	7-6" 75	10'-0"
2000 paf	1'-3"	6'-6" 60	INC.	1'-10"	50 1'-9"	2'-9" 3	1'-6"	8'-0" 73	11'-0"
		GENANA S	Versia de la		UYERIA	DEBION C	TAL	AT SECTION	
		EUROHURSE	SLOPE OF WILL	ANGLE BASE	PRESSURE PRESSURE 44	ACTIVE PRESSURE	SLOPE BOT	SLOPE TOP	SEASON Qu
		250 per	99.46 deg	17 dea	26 deg	26 deg	7.13 dag	0 deg	500PSF

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REMAINS WITH THE DESIGN ENGINEER. THE CITY OF ROCKWALL, IN REVIEWING AND RELEASING PLANS FOR CONSTRUCTION, ASSUMES NO RESPONSIBILITY FOR ADEQUACY OR ACCURACY OF DESIGN.

ALL RESPONSIBILITY FOR ADEQUACY OF DESIGN

GITY OF HOCKWALL ENGINEERING DEPT.

5-27-21 DATE

AARON M. BERKES

WALLCO RETAINING WALLS, 4800 S.E. LOOP 820 FORT WORTH, TEXAS 76140

DES. ORN.

Falkofske Engineering, Inc.
Structural Engineering Consultants
TX Reg. Engineering Firm F-4038
722 North Fielder Road
Arlington, Texas 76012
(817) 261-8300

The use of these plans and peakerficial as peakerficial and has been stricted to the original site for which improposation would have been appeared to the original site for which the appear the peakerficial appropriate to the peakerficial appeared to the peakerficial and the peakerficial appropriate to the peakerficial proprieting of a specification contain proprieting and peakerficial appropriate the peakerficial pea

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MASONRY RETAINING V HARBOR HILLS SUMMER LEE DRIVE ROCKWALL, TEXAS

1 RW6

TYPICAL WALL SECTION - 250PSF FIRELANE SURCHARGE

1V:10H MAX SLOPE ABOVE WALL, 1V:8H MAX SLOPE BELOW WALL
BEARING IN CLAYEY SOILS